



STANFORD RSL TECH REPORT #67-4

"COMPUTER REDUCTION AND ANALYSIS  
OF AN INFRARED IMAGE"

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by

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December 31, 1967

REMOTE SENSING LABORATORY  
GEOPHYSICS DEPARTMENT

STANFORD UNIVERSITY • STANFORD, CALIFORNIA

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Already Issued

67-1 "Field Infrared Analysis of Terrain - Spectral Correlation  
Program" Part I

67-2 "Field Infrared Analysis of Terrain - Spectral Correlation  
Program" Part II and Part III

67-3 "Statistical Analysis of IR Spectra - Stanford Programs  
Applied to USGS Spectra in Tech Letter #13"

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31 December 1967

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## I. ABSTRACT

Raw infrared scan imagery comprises three variables - two direction dimensions and film tone. Film tone, or density, may be reduced to absolute temperature by digitizing the data (manually or by machine) and submitting it to a computer. A Fortran IV program has been written for the IBM 7090 to accomplish this. Another program is included which fits a three-dimensional trend surface to the temperature data and computes thermal residuals. The trend surface maps define temperature patterns, and thermal residual maps isolate local anomalies.

As an illustration, one infrared image is followed through the reduction and analysis procedure, from film to isothermal, trend and residual maps. The total cost for one complete run was \$80.

## II. INTRODUCTION

With most remote sensing systems, data are generated faster than they can be reduced. Computers must be used in the reduction process.

This paper describes methods developed to reduce an infrared image to an isothermal map and to analyse temperature data by trend surface fitting. The imagery used was produced by a relatively slow, fixed-position scanner, but with appropriate modifications the same procedures should be applicable to airborne scan imagery.

### Scanner

The infrared scanner used was the Barnes T-4 infrared camera. This camera is made up of an optical head (the scanning system and radiometer) and an electronics unit. The system gathers incoming radiation and reflects it from a plane mirror into the radiometer, which is the Barnes R8T 8-inch (thermistor bolometer). The plane mirror is mechanically oscillated to scan the field in horizontal sweeps. The field of view is  $10^\circ$  by  $20^\circ$ , composed of approximately 180 horizontal traverses. Radiation from the scan mirror is focused on the detector by Cassegrain optics through a filter which cuts off short wavelength radiation ( $< 5\mu$ ), with an optical resolution (instantaneous f.o.v.) of 1 milliradian. The incident radiation is periodically cut out by a chopper, which in turn reflects radiation from a known temperature blackbody onto the detector. This blackbody radiation is used as a reference to which the incident radiation is compared. Target temperature differences which exceed the system noise (Noise Equivalent Temperature Difference) are  $0.04^\circ\text{C}$  at a chop frequency of 1 cps and  $0.3^\circ\text{C}$  at 50 cps. A preamplifier feeds the electric signal from the detector to the electronics unit, which in turn activates a glow tube whose intensity is approximately linearly proportional to the absolute value of the incident thermal radiation. An attenuation circuit and a temperature offset circuit are operator-controlled to adjust the system to the range of incident radiation. The light from the glow

tube is collimated by a lens and aperture into a narrow beam directed at a mirror attached to the back of the target-scanning mirror, from which it is reflected to Polaroid Positive/Negative film. As the mirror system oscillates, the variable intensity light beam thus "writes" the image in raster form. The final image comprises 60,000 bits, or individual temperature measurements, recorded in six minutes.

A step-voltage mechanism produces a stepped gray scale at the top of the photo for calibration.

Image

Fig. 1 is an infrared image of a pan of water approximately 1.2 meters in diameter. The image was recorded during a series of experiments with the Barnes imager conducted at the Stanford Remote Sensing Laboratory in 1967.

The target is a standing body of water in a circular evaporation pan. A constant point discharge of warmer water is being introduced to the water surface at the bottom of the image, as shown by the lighter tone. This image was made from a point 7 meters above the target at a look angle of 14-24° from vertical.

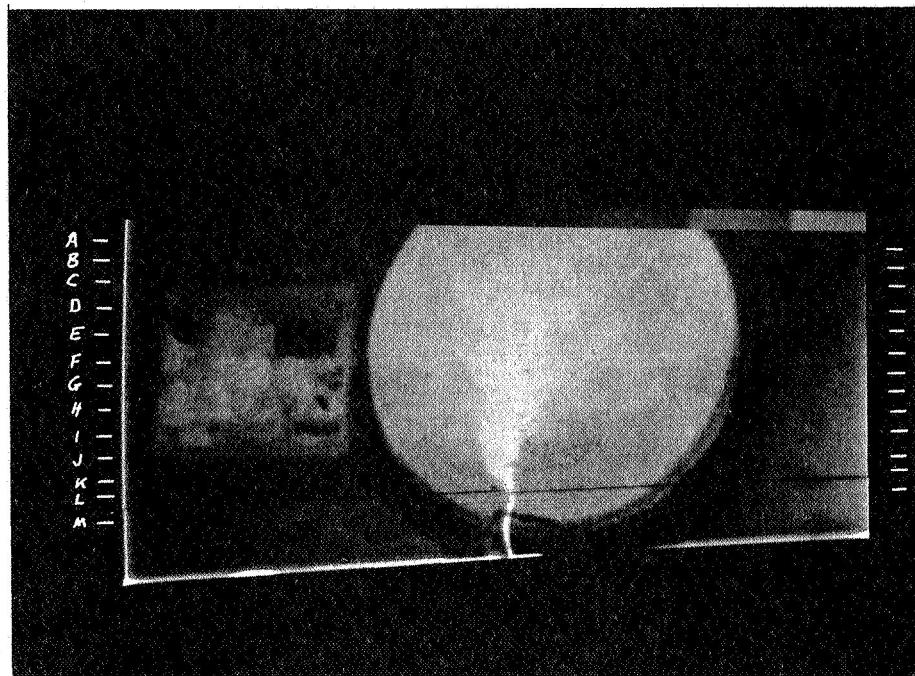


Fig. 1 Infrared image of standing body of water with point discharge of warmer water. Discharge is constant from point at lower edge of pan. Water body 1.2m diameter,  $0.3\text{m}^3$ . Look angles  $14-24^\circ$ . Fiducial marks are density profile indices. Image from Barnes camera,  $5-20\mu$ , 6 minute scan.

### III. DIGITIZING METHODS

The raw data format of most IR scanner systems is a photo negative consisting of three variables - x,y and photo density. The first reduction process is therefore the quantification of photo density. Lacking such instruments as a dual beam scanning microdensitometer, the method used here was to measure the photo density of the negative along a series of profiles. This was done using a Jarrell-Ash Microphotometer with a strip chart recorder; an example of the output is shown in Fig. 2. Each profile represents a row of an infinite number of density values  $D_{x_1y}$ ,  $D_{x_2y} \dots D_{x_ny}$ . At regular or irregular increments of x, the density is determined (density scale is arbitrary, but must be identical to that used for the calibration gray scale), either manually or by use of a digitizer. The latter method was used for this program, but manual means appear more efficient unless a large number of profiles or a large number of data points for each profile is required. In this case, the optical density profiles were digitized on a Calma digitizer, which reads every 0.01 inch and records on half-inch magnetic tape on a Kennedy incremental tape recorder in BCD form. Data from each profile are recorded in a single file block with their appropriate alphabetic identifier. The digital tape is then used as input with an interpolation program which determines the dependent variable (density) for any specified increment of independent variable (x). Each data point (x,y density) is punched on a card and forms the basic input for the computer program to follow.

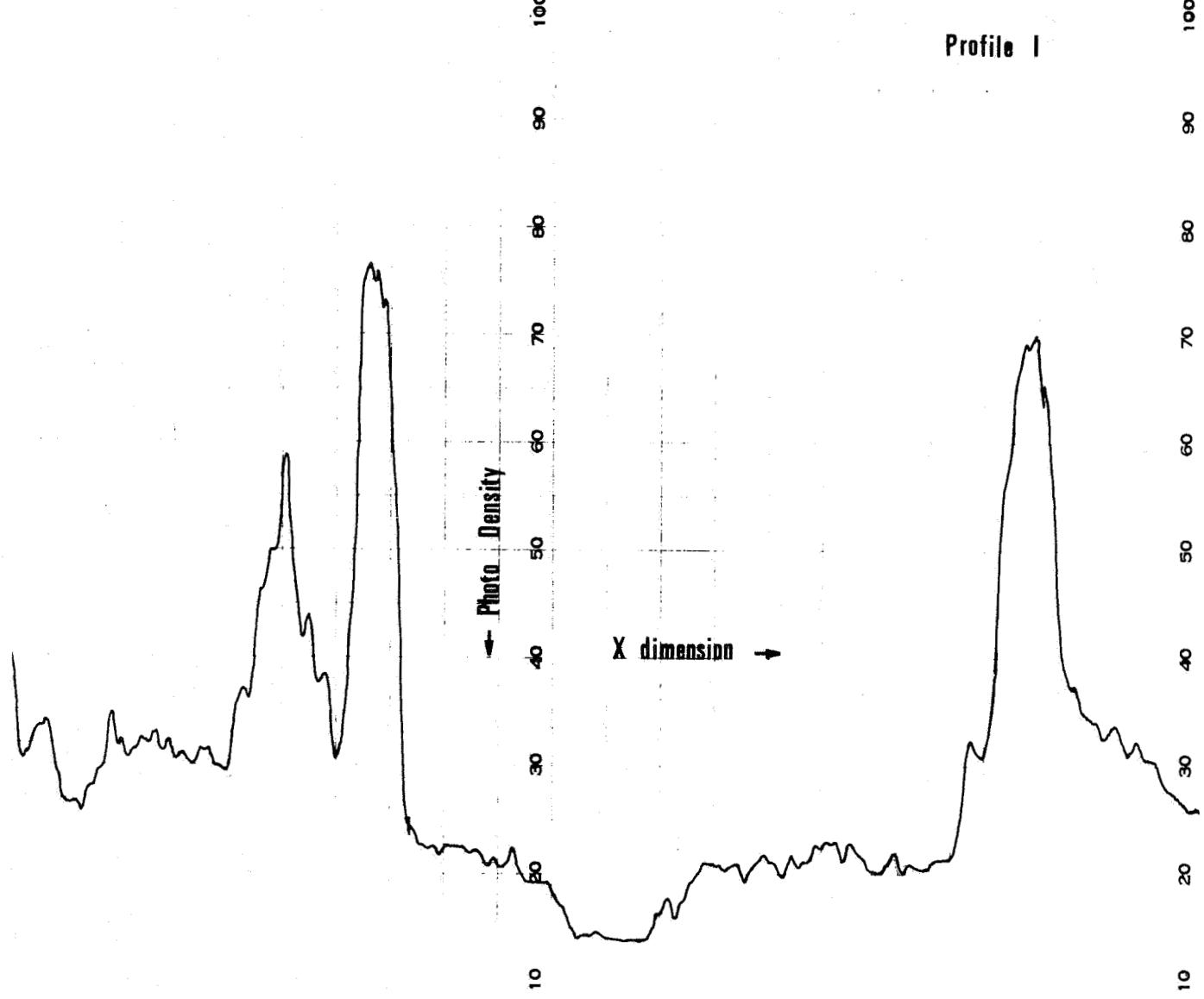


Fig. 2-Optical density profile.

#### IV. COMPUTER PROGRAMS

The computer programs are written in Fortran IV for the IBM 7090. A listing of each program is in the Appendix, along with an example of input and output. In these programs, the one example of infrared imagery already discussed is followed through the programs, from image density to thermal trends and residuals.

##### A. Photo Density Reduction Program

This program essentially converts the third input variable of each data point, density, to absolute temperature. The basic steps are:

1. For each data point, the density is assigned a gray scale value by interpolation or extrapolation of the density vs. calibration gray scale curve.
2. From the determined gray scale value, the current (to the light source) is found by interpolation/extrapolation of a gray scale vs. current curve.
3. The current value - along with the instrument constants, gain settings, etc. - determines the radiance by mathematical computation.
4. Absolute temperature is found by interpolation/extrapolation of a radiance vs. temperature curve.
5. The three variables for each data point, now x,y and temperature, are written out and/or punched on cards.

A flow chart of the program is shown in Fig. 3. Appendices A,B and C are the program listing, input and output.

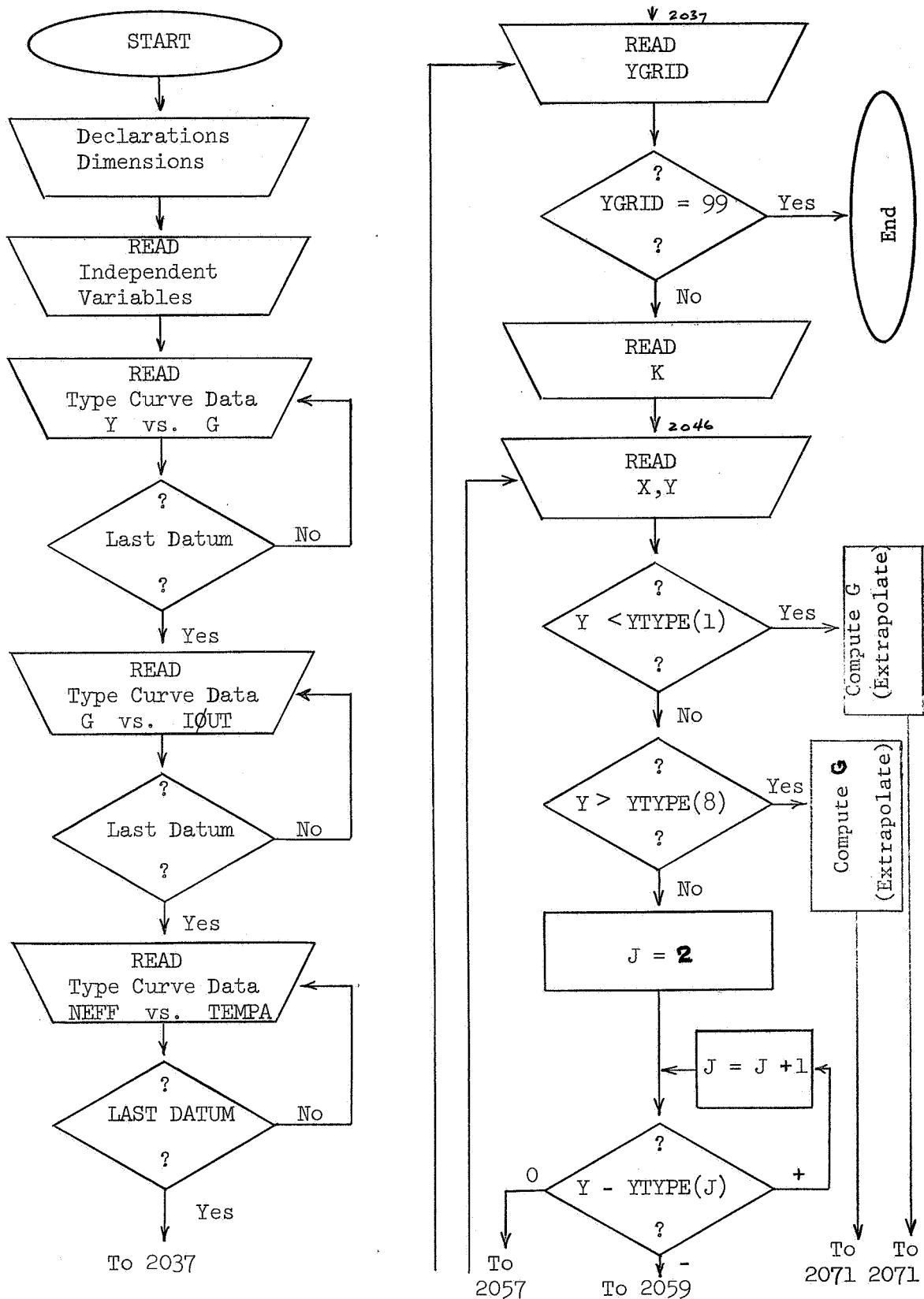


Fig. 3 Photo Density Reduction program.

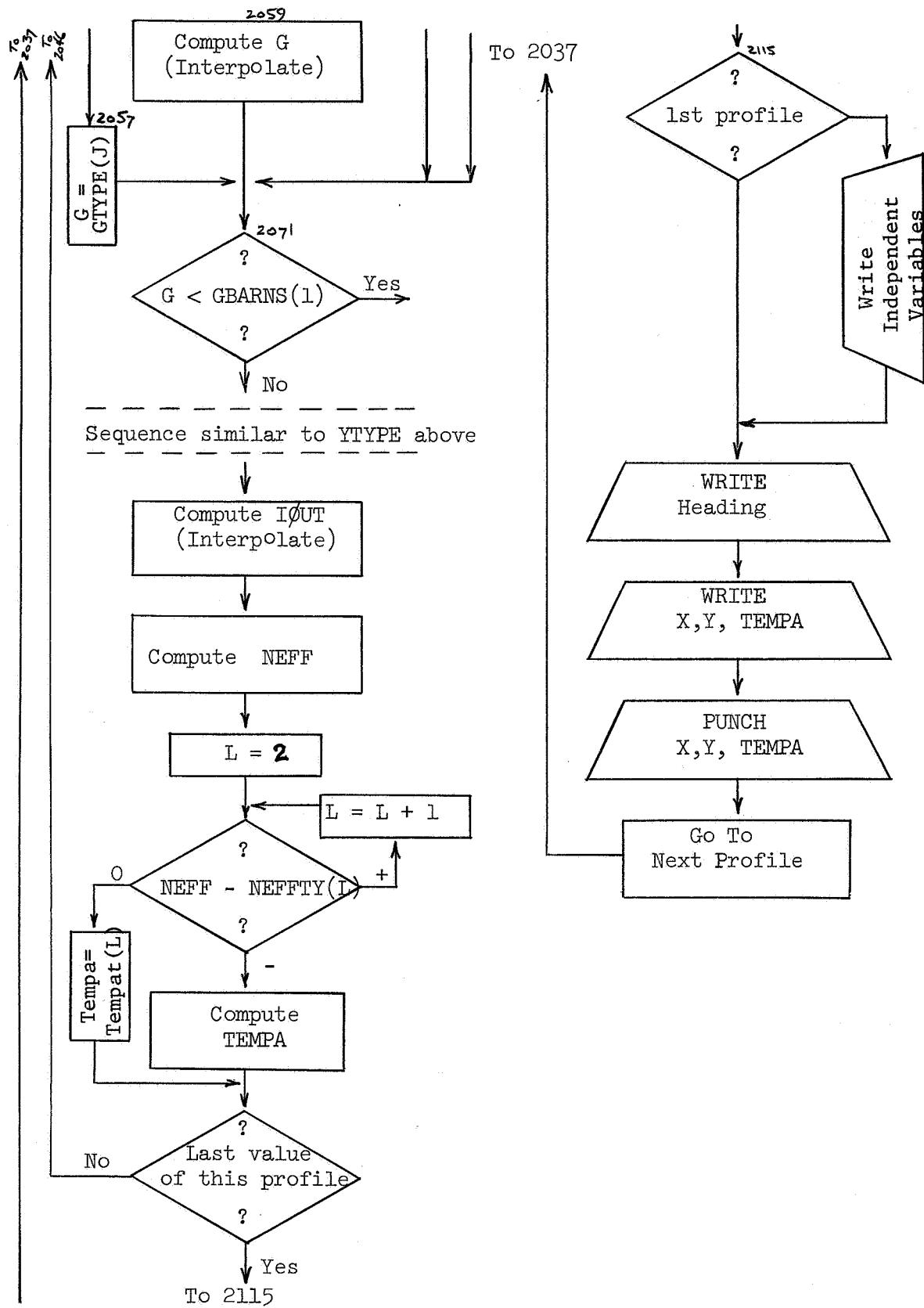


Fig. 3 (cont'd.)

## B. Trend Surface/Residual Program

Once imagery has been reduced to absolute temperature, it remains to analyze and display the data. An attempt was made to analyze the data by fitting trend surfaces and determining residuals. In the application of this method to water surface temperatures, broad patterns are more clearly defined by trend surfaces and local anomalies are isolated as residuals.

The trend surface program fits a geometric surface to the observed data by satisfying the least squares criterion. The surfaces fitted by this program are planar, parabolic and hyperbolic, whose equations are:

first degree surface (planar)

$$W_{\text{trend}} = A + Bx + Cy$$

second degree surface (parabolic)

$$W_{\text{trend}} = A + Bx + Cy + Dx^2 + Exy + Fy^2$$

third degree surface (hyperbolic)

$$\begin{aligned} W_{\text{trend}} = & A + Bx + Cy + Dx^2 + Exy + Fy^2 + Gx^3 + Hx^2y \\ & + Ixy^2 + Jy^3 \end{aligned}$$

To minimize the sum of the squared deviations (where deviation =  $W_{\text{observed}} - W_{\text{trend}}$ ), the latter are expressed as functions of A,B,C...,

$$F(A,B,C...) = \sum (W_{\text{observed}} - A - Bx - Cy - \dots)^2,$$

and the partial derivatives of F with respect to A,B,C... are set equal to zero. If the summed terms are written in matrix equation form, the coefficients may be obtained by matrix inversion and division (Sub-routine SOLVE). Fig. 4 is the matrix form for a third degree surface.

$$\begin{bmatrix}
 \Sigma N & \Sigma x & \Sigma y & \Sigma x^2 & \Sigma xy & \Sigma y^2 & \Sigma x^3 & \Sigma x^2 y & \Sigma xy^2 & \Sigma y^3 \\
 \Sigma x^2 & \Sigma xy & \Sigma x^3 & \Sigma x^2 y & \Sigma xy^2 & \Sigma x^4 & \Sigma x^3 y & \Sigma x^2 y^2 & \Sigma xy^3 & \\
 \Sigma y^2 & \Sigma x^2 y & \Sigma xy^2 & \Sigma y^3 & \Sigma x^3 y & \Sigma x^2 y^2 & \Sigma xy^3 & \Sigma y^4 & \\
 \Sigma x^4 & \Sigma x^3 y & \Sigma x^2 y^2 & \Sigma x^5 & \Sigma x^4 y & \Sigma x^3 y^2 & \Sigma x^2 y^3 & \Sigma xy^4 & \\
 \Sigma x^2 y^2 & \Sigma xy^3 & \Sigma x^4 y & \Sigma x^3 y^2 & \Sigma x^2 y^3 & \Sigma xy^4 & \Sigma y^5 & \\
 \Sigma y^4 & \Sigma x^3 y^2 & \Sigma x^2 y^3 & \Sigma xy^4 & \Sigma y^5 & \Sigma x^6 & \Sigma x^5 y & \Sigma x^4 y^2 & \Sigma x^3 y^3 \\
 \Sigma x^4 y^2 & \Sigma x^3 y^3 & \Sigma x^3 y^4 & \Sigma x^2 y^4 & \Sigma xy^5 & \Sigma x^4 y^2 & \Sigma x^5 y & \Sigma x^4 y^3 & \\
 \Sigma x^2 y^5 & \Sigma xy^6 & \Sigma y^6 & & & \Sigma z & \Sigma zy & \Sigma zx & \Sigma zy^3 \\
 \end{bmatrix} = \begin{bmatrix}
 A & \Sigma z \\
 B & \Sigma zx \\
 C & \Sigma zy \\
 D & \Sigma zx^2 \\
 E & \Sigma zxy \\
 F & \Sigma zy^2 \\
 G & \Sigma zx^3 \\
 H & \Sigma zx^2 y \\
 FI & \Sigma zxy^2 \\
 FJ & \Sigma zy^3
 \end{bmatrix}$$

Fig. 4 Matrix equation for third degree trend surface.

With the coefficients determined, the value of  $W_{trend}$  is computed for each map co-ordinate and "plotted" on the line printer.

Residual values are computed as the difference, at each data point, between the observed temperature and the trend surface temperature.

Fig. 5 is a flow chart of this program. Appendices D-G are program listings, input and output examples.

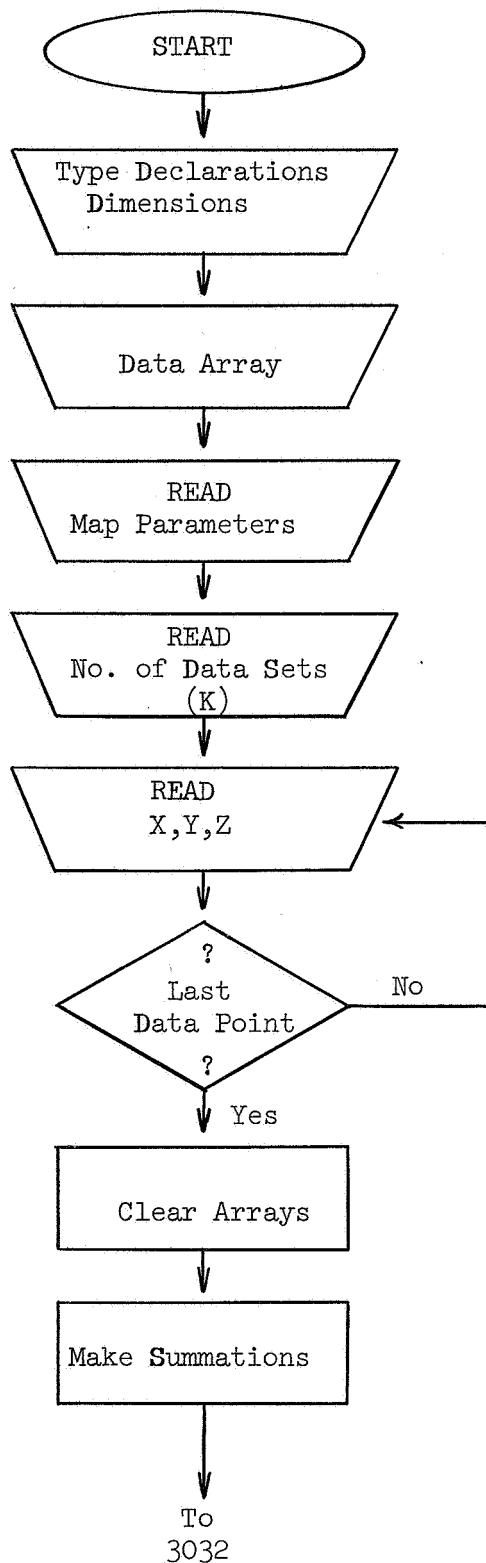


Fig. 5 Trend Surface/Residual program  
-12-

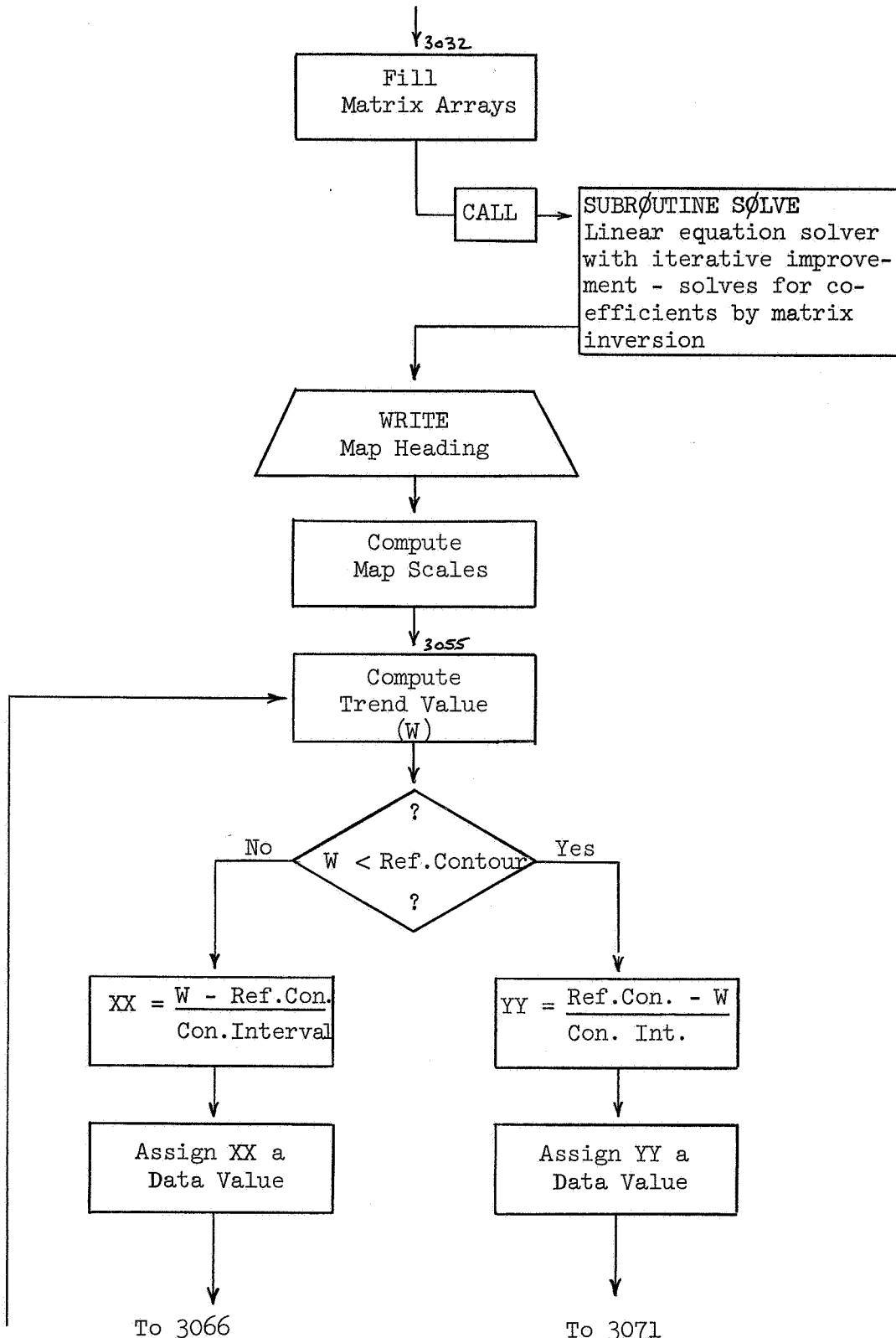


Fig. 5 (cont'd.)

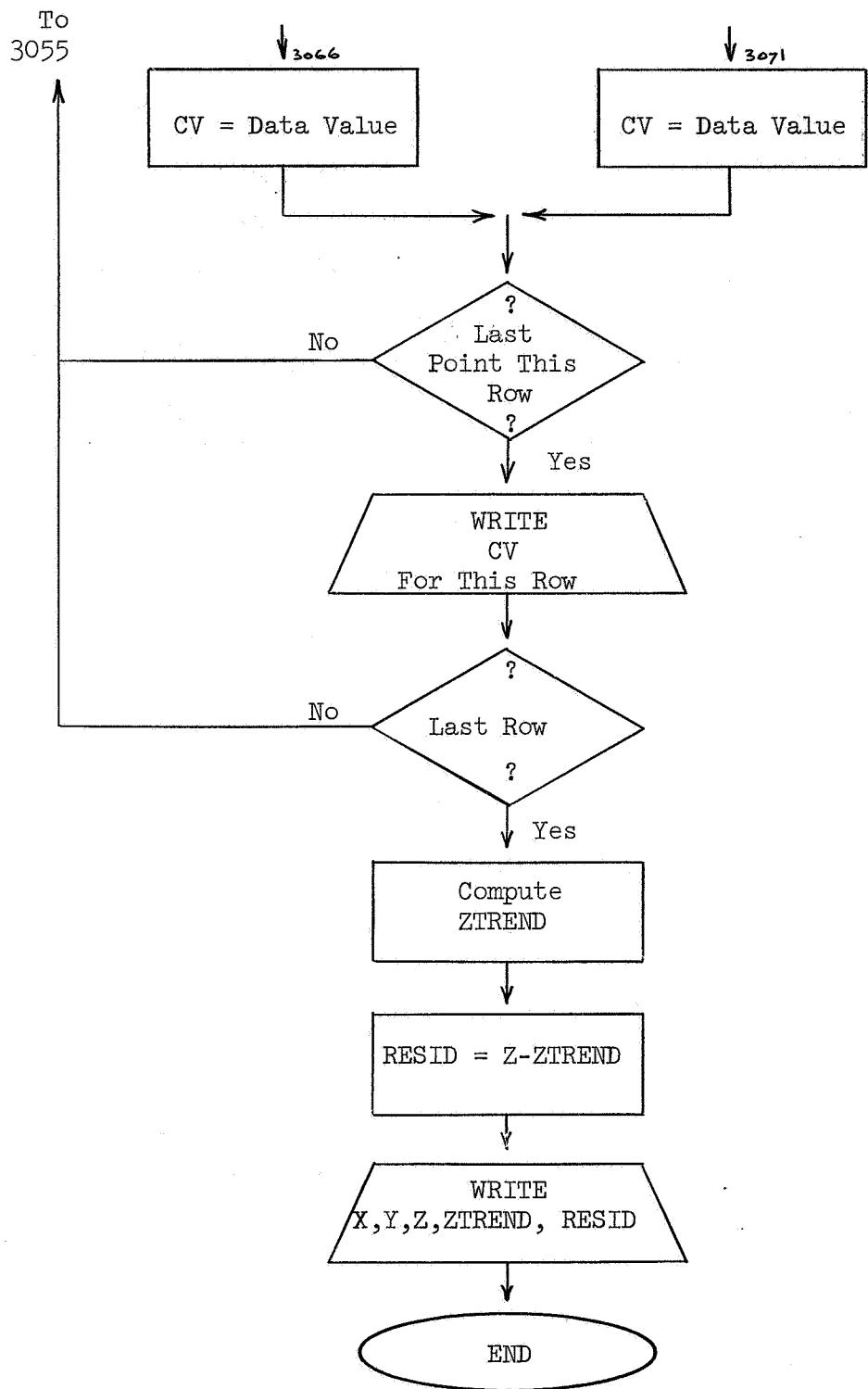


Fig. 5 (Cont'd.)

## V. DISPLAY

Data, whether computed temperatures or residuals, may be displayed simply by plotting the values on an x-y grid and contouring the values. This may be done manually or by computer. Hand contouring is perhaps neater, but the computer is certainly more objective. Appendix H contains examples of Calcomp contour maps of temperatures and thermal residuals. The plotting program was obtained from Dr. Graham Bonham-Carter of the Department of Geology, Stanford University.

## VI. TIME/COST

### Densitometer Profiles

Density profiles are time-consuming. Set-up time is about equal to the warm-up time of the microphotometer - 30 minutes. As with other methods, the time-per-unit decreases as the number of units increases. For 13 profiles, total time was 1.7 man-hours:

$$\text{Time} \doteq (0.5 + (13 \text{ profiles} \cdot 5.5 \text{ min/prof})/60) = \underline{1.7 \text{ hours}}$$

### Digitizing

Density profiles in small numbers are more efficiently digitized by hand than by machine. The crossover between small and large numbers, of course, depends on the cost of computer time, wage rates and the number of points to be digitized per profile. For the case in point, where about 13 data points were used from each profile, the crossover is at about 20 profiles. The comparison is made:

#### Hand digitized

$$\begin{aligned} \text{Time} &\doteq (13 \text{ prof} \cdot 15 \text{ min/prof})/60 = 3.25 \text{ man-hours (for}} \\ &\quad \text{digitizing)} \end{aligned}$$

$$\begin{aligned} \text{Time} &\doteq (184 \text{ data points} \cdot 0.147 \text{ min/dp})/60 = .45 \text{ m-h (for key-}} \\ &\quad \text{punch)} \end{aligned}$$

$$\text{Total} = 3.70 \text{ m-h} \cdot \$4.50/\text{hr} = \underline{\underline{\$ 16.60}}$$

#### Machine digitized

$$\text{Time} \doteq (0.4 + (13 \text{ prof} \cdot 7.2 \text{ min/prof})/60) = 2.0 \text{ m-h}$$

$$\text{Computer total use time} \doteq 3.0 \text{ min}$$

$$\begin{aligned} \text{Total} &= 2.0 \text{ m-h} \cdot \$4.50/\text{hr} + 3.0 \text{ min} \cdot \$3.75/\text{min} \\ &= \underline{\underline{\$ 20.25}} \end{aligned}$$

### Computer Programs

Following are the total computer use times for each program segment

(for 184 data points). The computer used was an IBM 7090.

Photo Density Reduction	0 min	36 sec
1st Trend Surface/Residual	0	54
2nd Trend Surface/Residual	1	02
3rd Trend Surface/Residual	1	06
Plot Isotherms	3	00
Plot 1st Residuals	2	21
Plot 2nd Residuals	2	17
Plot 3rd Residuals	2	32

Normally, not all of the above segments would be used. For a complete run of all segments (without splicing), the total machine time would be 13.80 minutes, or, at \$225/hr, \$51.75.

```

C PROGRAM TO REDUCE PHOTO INTENSITY TO TARGET TEMPERATURE          2001
C -----                                                               2002
C                                                               2003
C         INTEGER YGRID                                              2003A
C         REAL NREF,NEFF,KS,IOUTBA,NEFFTY,TOUT                         2004
C         DIMENSION YTYPE(8),GTYPE(8),GBARNS(8),IOUTBA(8),NEFFTY(21),TEMPAT 2005
C         -(21),X(100),Y(100),G(100),TOUT(100),TEMPA(100),TEMPT(100),NEFF 2006
C         -(100)                                                       2006A
C
C-----                                                               2007
C-----                                                               2008
C READ INDEPENDENT VARIABLES                                     2009
C-----                                                               2010
C         READ(5,50) KS,S,GAIN,TSKY,VETO,SF,EMISS,TAU,NREF,SIGMA        2011
C         50 FORMAT (5F6.1,3F6.3,F7.5,E10.4)                                2012
C
C-----                                                               2013
C-----                                                               2014
C DEFINE TYPE CURVE OF Y VS. G                                 2015
C-----                                                               2016
C         DO 1 I=1,8                                              2017
C         1 READ(5,51) YTYPE(I),GTYPE(I)                                2018
C         51 FORMAT (2F5.1)                                         2019
C
C-----                                                               2020
C-----                                                               2021
C DEFINE TYPE CURVE OF G VS. ICUT                            2022
C-----                                                               2023
C         DO 2 I=1,8                                              2024
C         2 READ(5,51) GBARNS(I),IOUTBA(I)                                2025
C
C-----                                                               2026
C-----                                                               2027
C DEFINE TYPE CURVE OF NEFF VS. TEMPAT                      2028
C-----                                                               2029
C         DO 3 I=1,21                                             2030
C         3 READ(5,52) NEFFTY(I),TEMPAT(I)                                2031
C         52 FORMAT(F7.5,F6.1)                                         2032
C         ICOUNT=1                                                 2033
C
C-----                                                               2034
C COMPUTE ALL VALUES FOR ONE PROFILE (ONE YGRID)           2035
C-----                                                               2036
C
C         4 READ(5,53) YGRID                                         2037
C         53 FORMAT (I3)
C         IF (YGRID.EQ.99) GO TO 999                                2038
C
C-----                                                               2039
C         NUMBER OF DATA POINTS (K) IN ONE PROFILE                 2040
C-----                                                               2041
C
C         READ(5,54) K                                         2042
C         54 FORMAT (I3)
C         DO 1000 I=1,K                                         2043
C         READ(5,55) X(I),Y(I)                                    2044
C         55 FORMAT (I4,F5.1)                                         2045
C
C-----                                                               2046
C         INTERPOLATE TO FIND GRayscale VALUE (G)                2047
C-----                                                               2048
C
C         IF(Y(I).LT.YTYPE(1)) GO TO 104                           2049
C-----                                                               2050
C-----                                                               2051

```

```

        IF(Y(I).GT.YTYPE(8)) GO TO 105          2052
        J=2                                     2053
100  IF(Y(I)=YTYPE(J)) 103,102,101          2054
101  J=J+1                                    2055
     GO TO 100                                2056
102  G(I) = GTYPE(J)                         2057
     GO TO 200                                2058
103  G(I) = GTYPE(J-1) +(GTYPE(J)-GTYPE(J-1))/(YTYPE(J)-YTYPE(J-1))*Y(2059
     -I)-YTYPE(J-1))                          2060
     GO TO 200                                2061
104  G(I) = GTYPE(1)-(GTYPE(2)-GTYPE(1))/(YTYPE(2)-YTYPE(1))*(YTYPE(1)-2062
     -Y(I))                                  2063
     GO TO 200                                2064
105  G(I) = GTYPE(8)+(GTYPE(8)-GTYPE(7))/(YTYPE(8)-YTYPE(7))*(Y(I)-YTYPE(7)-E(R)) 2065
     GO TO 200                                2066
C -----
C INTERPOLATE TO FIND CURRENT (IOUT)        2067
C -----
200  IF(G(I).LT.GBARNs(1)) GO TO 205          2068
     IF(G(I).GT.GBARNs(8)) GO TO 206          2069
     N=2                                     2070
201  IF(G(I)=GBARNs(N)) 204,203,202          2071
202  N=N+1                                    2072
     GO TO 201                                2073
203  IOUT(I)=IOUTBA(N)                      2074
     GO TO 300                                2075
204  IOUT(I)=IOUTBA(N-1)+(IOUTBA(N)-IOUTBA(N-1))/(GBARNs(N)-GBARNs(N-1)) 2076
     *(G(I)-GBARNs(N-1))                      2077
     GO TO 300                                2078
205  IOUT(I)=IOUTBA(1)-(IOUTBA(2)-IOUTBA(1))/(GBARNs(2)-GBARNs(1))*(GBA2079
     -RNS(1)-G(I))                           2080
     GO TO 300                                2081
206  IOUT(I)=IOUTBA(8)+(IOUTBA(8)-IOUTBA(7))/(GBARNs(8)-GBARNs(7))*(G(I2082
     -)-GBARNs(8))                           2083
     GO TO 300                                2084
C -----
C COMPUTE EFFECTIVE RADIANCE (NEFF)          2085
C -----
300  NEFF(I)=NREF+((S*IOUT(I))/GAIN-VETO)/(KS*SF*1000.0) 2086
C -----
C INTERPOLATE TO FIND APPARENT TEMPERATURE (TEMPA) 2087
C -----
L=2                                     2088
400  IF(NEFF(I)=NEFFT(Y(L))) 403,402,401 2089
401  L=L+1                                    2090
     GO TO 400                                2091
402  TEMPAT(I)=TEMPAT(L)                      2092
     GO TO 1000                               2093
403  TEMPAT(I)=TEMPAT(L-1)+(TEMPAT(L)-TEMPAT(L-1))/(NEFFT(Y(L))-NEFFT(Y(L-12101
     -)))*(NEFF(I)-NEFFT(Y(L-1)))           2102
1000 CONTINUE                            2110
C -----
C -----                                     2111
C -----                                     2112
C WRITE OUT ALL VALUES FOR THIS PROFILE      2113

```

```

C -----
      IF(ICOUNT.GT.1) GO TO 600                                2114
      WRITE(6,60)                                               2115
 60 FORMAT(1H1)                                               2116
      WRITE(6,61)                                               2117
 61 FORMAT(64H   KS     S    GAIN   TSKY   VETO   SF    EMISS   TAU   NREF 2118
      -   SIGMA)                                              2119
      WRITE(6,50) KS,S,GAIN,TSKY,VETO,SF,EMISS,TAU,NREF,SIGMA 2120
 600 WRITE(6,60)                                               2121
      WRITE(6,62)                                               2122
 62 FORMAT (63H       X        Y        TEMPA      GRAY      IOUT 2123
      -   NEFF )                                              2124
      WRITE (6,63)                                              2125
 63 FORMAT(57H ..... 2126
      -.)                                                 2127
      WRITE (6,64)                                              2128
 64 FORMAT(1H //)                                              2129
      DO 2000 I=1,K                                           2130
      F(I) = X(I)                                             2131
 2000 WRITE (6,65) F(I),YGRID,TEMPA(I),G(I),IOUT(I),NEFF(I) 2132
 65 FORMAT (3F10.1,2F10.2,F12.6)                            2133
      DO 2001 I=1,K                                           2133A
 2001 WRITE (6,66) F(I),YGRID,TEMPA(I),G(I),IOUT(I),NEFF(I) 2133B
 66 FORMAT (1HP,3F10.1,2F10.2,F12.6)                         2133C
      ICOUNT=ICOUNT+1                                         2134
C -----
C GO TO NEXT PROFILE                                         2135
C -----
      GO TO 4                                                 2136
C
 999 RETURN                                                 2137
      END                                                       2138
                                         2139
                                         2140
                                         2141

```

117.8	44.6	3.6	296.5	160.0	1,233	.980	1,000	.00758	.5673E-11	IND VAR
21.0	1.0									Y/G TYPE
30.0	2.0									Y/G TYPE
40.0	3.0									Y/G TYPE
51.8	4.0									Y/G TYPE
68.0	5.0									Y/G TYPE
81.6	6.0									Y/G TYPE
90.0	7.0									Y/G TYPE
95.3	8.0									Y/G TYPE
1.0	25.0									G/I TYPE
2.0	18.5									G/I TYPE
3.0	12.4									G/I TYPE
4.0	8.9									G/I TYPE
5.0	5.9									G/I TYPE
6.0	3.6									G/I TYPE
7.0	2.2									G/I TYPE
8.0	1.2									G/I TYPE
.00502	0.0									N/T TYPE
.00548	5.0									N/T TYPE
.00598	10.0									N/T TYPE
.00646	15.0									N/T TYPE
.00700	20.0									N/T TYPE
.00758	25.0									N/T TYPE
.00820	30.0									N/T TYPE
.00882	35.0									N/T TYPE
.00956	40.0									N/T TYPE
.01006	45.0									N/T TYPE
.01110	50.0									N/T TYPE
.01190	55.0									N/T TYPE
.01280	60.0									N/T TYPE
.01370	65.0									N/T TYPE
.01470	70.0									N/T TYPE
.01560	75.0									N/T TYPE
.01660	80.0									N/T TYPE
.01770	85.0									N/T TYPE
.01880	90.0									N/T TYPE
.02000	95.0									N/T TYPE
.02120	100.0									N/T TYPE
46										YGRID
26										K YGRID46
0	47.0									Y DATA YGRID46
5	43.0									
11	40.6									
16	40.0									
18	30.5									
21	23.1									
26	23.4									
32	28.0									
34	37.2									
37	30.0									
40	28.9									
45	29.0									
47	29.0									
50	36.1									
53	37.2									
55	30.1									

61 31.0  
66 32.5  
68 38.7  
74 55.1  
79 60.2  
82 62.8  
84 57.3  
87 42.3  
95 35.2  
99 28.6

76

21

0 42.7  
3 43.8  
5 31.1  
11 27.0  
13 41.8  
16 43.6  
21 24.5  
29 23.6  
34 39.2  
37 28.0  
42 29.6  
47 27.8  
52 39.9  
55 32.2  
63 33.0  
68 41.6  
74 64.0  
79 69.4  
84 64.1  
87 44.0  
95 38.7  
99

YGRID  
K YGRID76  
Y DATA YGRID76

YGRID

KS	S	GAIN	TSKY	VETO	SF	EMISS	TAU	NREF	SIGMA
117.8	44.6	3.6	253.0	90.0	1.098	0.980	1.000	0.00673	0.5673E-11

X	Y	TEMPA	GRAY	IOUT	NEFF
0.	2.2	32.3	0.90	25.65	0.008491
10.0	2.2	32.3	0.90	25.65	0.008491
20.0	2.2	33.4	0.70	26.95	0.008616
30.0	2.2	33.2	0.73	26.73	0.008595
40.0	2.2	33.7	0.63	27.38	0.008657
50.0	2.2	34.0	0.57	27.82	0.008699
60.0	2.2	33.4	0.68	27.06	0.008626
70.0	2.2	34.9	0.38	29.01	0.008813
80.0	2.2	33.3	0.72	26.84	0.008605
90.0	2.2	32.8	0.82	26.19	0.008543
100.0	2.2	33.1	0.75	26.63	0.008584
110.0	2.2	32.6	0.85	25.97	0.008522
120.0	2.2	32.7	0.83	26.08	0.008533

```

C FIRST DEGREE TREND SURFACE W/ FIRST DEGREE RESIDUALS      3001   1
C -----      3002
C -----      3003
C      INTEGER PLUS, MINUS, CV      3004
C      DIMENSION W(300),CV(300),PLUS(30),MINUS(30),AA( 3, 3),BB( 3),COEF(3005  1
C      - 3),X(300),Y(300),Z(300),RESID(300),ZTREND(300)      3006   1
C      DATA(PLUS(I),I=1,20)/1H ,1H ,1H2,1H ,1H3,1H ,1H4,1H ,1H5,1H ,1H6,1H ,1H7,1H ,1H8,1H ,1H9,1H ,1H0/, (MINUS(I),I=1,20)/1H ,1H1,1H ,21H2,1H ,1H3,1H ,1H4,1H ,1H5,1H ,1H6,1H ,1H7,1H ,1H8,1H ,1H9,1H ,1H10/      3007
C      3008
C      3009
C      30/
C      READ (5,50) HORZ,VERT,XL,XR,YT,YB,REF,CON      3010
C      50 FORMAT (8F6.1)      3011
C      READ (5,51) K      3012
C      51 FORMAT (I4)      3013
C      DO 200 I=1,K      3014
C      READ (5,8) X(I), Y(I), Z(I)      3015
C      8 FORMAT (3F10.1)      3016
C      200 CONTINUE      3017
C -----      3018
C      SET DEP VARIABLES = 0.0      3019
C -----      3020
C      3021
C      X1 =0.0      302201 1
C      X2 =0.0      302202 1
C      Y1 =0.0      302203 1
C      Y2 =0.0      302204 1
C      XY =0.0      302205 1
C      Z1 =0.0      302206 1
C      ZY =0.0      302207 1
C      ZX =0.0      302208 1
C -----      3023
C      MAKE SUMMATIONS      3024
C -----      3025
C      DO 100 I=1,K      3026
C      X1 = X1+X(I)      302701 1
C      X2 = X2+X(I)*X(I)      302702 1
C      Y1 = Y1+Y(I)      302703 1
C      Y2 = Y2+Y(I)*Y(I)      302704 1
C      XY = XY+X(I)*Y(I)      302705 1
C      Z1 = Z1 + Z(I)      302706 1
C      ZX = ZX+Z(I)*X(I)      302707 1
C      ZY = ZY+Z(I)*Y(I)      302708 1
C      100 CONTINUE      3028
C -----      3029
C      FILL ARRAY      3030
C -----      3031
C      RK=K      3032
C      AA(1,1)=RK      303301 1
C      AA(1,2)=X1      303302 1
C      AA(1,3)=Y1      303303 1
C      AA(2,1)=X1      303304 1
C      AA(2,2)=X2      303305 1
C      AA(2,3)=XY      303306 1
C      AA(3,1)=Y1      303307 1
C      AA(3,2)=XY      303308 1
C      AA(3,3)=Y2      303309 1

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```

      BB(1)= Z1          303310 1
      BB(2)= ZX          303311 1
      BB(3)= ZY          303312 1
C -----
C SOLVE FOR COEFFICIENTS BY MATRIX INVERSION          3034
C -----
C      CALL SOLVE (3,AA,BB,1,0,0,10,COEF,IT)          3035
C      A = COEF(1)          3036
C      B = COEF(2)          3037 1
C      C = COEF(3)          303801 1
C -----
C WRITE MAP HEADING          303802 1
C -----
C      WRITE(6,996)          303803 1
996 FORMAT (1H1,52HW= A + BX + CY          FIRST DEGREE TREND 304301 1
  *D)
      WRITE(6,98)A,B,C          304302 1
98 FORMAT(1H ,8HWHERE A=, F15.8,5X,2HB=,F15.8,5X,2HC=,F15.8)          304303 1
      WRITE(6,97)HORZ,VERT          304304 1
97 FORMAT(1H ,27HARRAY DIMENSIONS ARE==HORZ=, F6.0,11H AND VERT=,F8.3044
  10)
      WRITE(6,96)XL,XR,YT,YB,REF,CON          3045
96 FORMAT(1H ,3HXL=,F10.2,10X,3HXR=,F10.2,10X,3HYT=,F10.2,10X,3HYB=, 3046
  1F10.2,10X,4HREF=,F10.2,10X,4HCON=,F10.2//)          3047
C -----
C FIRST DEGREE TREND SURFACE          3048
C -----
C      DX=(XR-XL)/HORZ          3049
C      DY=(YB-YT)/VERT          3050
C      IHORZ=HORZ          3051 1
C      IVERT=VERT          3052
C      DO 1 I=1,IVERT          3053
C      RI=I          3054
C      DO 2 J=1,IHORZ          3055
C      RJ=J          3056
C      W(J)=A+B*DX*RJ+C*DY*RI          3057
C      IF(W(J),LT,REF) GO TO 3          3058
C      XX=(W(J)-REF)/CON          3059
C      IX=XX          3060
C      IA=MUD(IX,20)          3061 1
C      CV(J)=PLUS(IA+1)          3062
C      GO TU 2          3063
3 YY=(REF-W(J))/CON          3064
IY=YY          3065
IB=MUD(IY,20)          3066
CV(J)=MINUS(IB+1)          3067
2 CONTINUE          3068
      WRITE(6, 95)(CV(K),K=1,IHORZ)          3069
95 FORMAT(1HT,132A1)          3070
1 CONTINUE          3071
C -----
C COMPUTE RESIDUAL VALUES          3072
C -----
C      DO 431 I= 1,K          3073
C      ZTREND(I)=A + B*X(I) + C*Y(I)          3074
C -----
C      3075
C -----
C      3076
C -----
C      3077
C -----
C      3078
C -----
C      3079
C -----
C      3080 1

```

```
431 RESID(I)=Z(I)=ZTREND(I)          3081
      WRITE (6,606)
606 FORMAT(1H1,51H      X      Y      Z      ZTREND 1ST=RESID) 3083   1
      DO 432 I=1,K
432 WRITE(6,607) X(I),Y(I),Z(I),ZTREND(I),RESID(I)          3084
607 FORMAT(1H ,5F10.1)          3085
102 RETURN          3086
      END          3087
                           3088
```

```

C 2ND DEGREE TREND SURFACE W/ 2ND DEGREE RESIDUALS      3001   2
C -----
C -----
C     INTEGER PLUS, MINUS, CV
C     DIMENSION W(300),CV(300),PLUS(30),MINUS(30),AA( 4, 4),BB( 4),COEF(3005  2
C     = 4),X(300),Y(300),Z(300),RESID(300),ZTREND(300)  3006
C     DATA(PLUS(I),I=1,20)/1H ,1H1,1H ,1H2,1H ,1H3,1H ,1H4,1H ,1H5,1H ,1H6,1H ,1H7,1H ,1H8,1H ,1H9,1H ,1H0/, (MINUS(I),I=1,20)/1H ,1H1,1H ,1H2,1H ,1H3,1H ,1H4,1H ,1H5,1H ,1H6,1H ,1H7,1H ,1H8,1H ,1H9,1H ,1H0/  3008
C     21H2,1H ,1H3,1H ,1H4,1H ,1H5,1H ,1H6,1H ,1H7,1H ,1H8,1H ,1H9,1H ,1H0/  3009
C     30/
C     READ (5,50) HORZ,VERT,XL,XR,YT,YB,REF,CON          3010
50 FORMAT (8F6.1)                                         3011
C     READ (5,51) K                                         3012
51 FORMAT (I4)                                         3013
C     DO 200 I=1,K                                         3014
C     READ (5,8) X(I), Y(I), Z(I)                         3015
8 FORMAT (3F10.1)                                         3016
200 CONTINUE                                              3017
C -----
C     SET DEP VARIABLES = 0.0                            3018
C -----
C     X4=0.0                                         3019
C     X3Y=0.0                                         3020
C     X2Y2=0.0                                         3021
C     X2=0.0                                         302201 2
C     XY3=0.0                                         302202 2
C     XY=0.0                                         302203 2
C     Y4=0.0                                         302204 2
C     Y2=0.0                                         302205 2
C     ZX2=0.0                                         302206 2
C     ZXY=0.0                                         302207 2
C     ZY2=0.0                                         302208 2
C     Z1=0.0                                         302209 2
C     Z1=0.0                                         302210 2
C     Z1=0.0                                         302211 2
C     Z1=0.0                                         302212 2
C -----
C     MAKE SUMMATIONS                                     3023
C -----
C     DO 100 I=1,K                                         3024
C     X4 = X4+X(I)*X(I)*X(I)*X(I)                      3025
C     X3Y = X3Y+X(I)*X(I)*X(I)*Y(I)                      3026
C     X2Y2= X2Y2+X(I)*X(I)*Y(I)*Y(I)                      302701 2
C     X2 = X2+X(I)*X(I)                                    302702 2
C     XY3 = XY3+X(I)*Y(I)*Y(I)*Y(I)                      302703 2
C     XY = XY+X(I)*Y(I)                                    302704 2
C     Y4 = Y4+Y(I)*Y(I)*Y(I)*Y(I)                      302705 2
C     Y2 = Y2+Y(I)*Y(I)                                    302706 2
C     ZX2 = ZX2+Z(I)*X(I)*X(I)                          302707 2
C     ZXY = ZXY+Z(I)*X(I)*Y(I)                          302708 2
C     ZY2 = ZY2+Z(I)*Y(I)*Y(I)                          302709 2
C     Z1 = Z1+Z(I)                                       302710 2
C     Z1 = Z1+Z(I)                                       302711 2
C     Z1 = Z1+Z(I)                                       302712 2
100 CONTINUE                                              3028
C -----
C     FILL ARRAY                                         3029
C -----
C     RK=K                                         3030
C     AA(1,1)=X"                                     3031
C     AA(1,1)=X"                                     3032
C     AA(1,1)=X"                                     303301 2

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AA(1,2)=X3Y	303302	2
AA(1,3)=X2Y2	303303	2
AA(1,4)=X2	303304	2
AA(2,1)=X3Y	303305	2
AA(2,2)=X2Y2	303306	2
AA(2,3)=XY3	303307	2
AA(2,4)=XY	303308	2
AA(3,1)=X2Y2	303309	2
AA(3,2)=XY3	303310	2
AA(3,3)=Y4	303311	2
AA(3,4)=Y2	303312	2
AA(4,1)=X2	303313	2
AA(4,2)=XY	303314	2
AA(4,3)=Y2	303315	2
AA(4,4)=RK	303316	2
BB(1)=ZX2	303317	2
BB(2)=ZXY	303318	2
BB(3)=ZY2	303319	2
BB(4)=Z1	303320	2
C -----	3034	
C SOLVE FOR COEFFICIENTS BY MATRIX INVERSION	3035	
C -----	3036	
CALL SOLVE (4, AA,BB,1,0,0,10,COEF,IT)	3037	2
A=COEF(1)	303801	2
B=COEF(2)	303802	2
C=COEF(3)	303803	2
D=COEF(4)	303804	2
C -----	3039	
C WRITE MAP HEADING	3040	
C -----	3041	
WRITE(6,996)	3042	
996 FORMAT(1H,28H SECOND DEGREE TREND SURFACE)	304301	2
WRITE(6,98)A,B,C,D	304302	2
98 FORMAT( 25HZ=AXX+BXY+CYY+D, WHERE A=, F15.8,5X,2HB=,F15.8,5X,	304303	2
12HC=,F15.8, 5X, 2HD=,F15.8 )	304304	2
WRITE(6,97)HORZ,VERT	3044	
97 FORMAT(1H ,27HARRAY DIMENSIONS ARE--HORZ=, F6.0,11H AND VERT=,F8.3045		
10)	3046	
WRITE(6,96)XL,XR,YT,YB,REF,CON	3047	
96 FORMAT(1H ,3HXL=,F10.2,10X,3HXR=,F10.2,10X,3HYT=,F10.2,10X,3HYB=,	3048	
1F10.2,10X,4HREF=,F10.2,10X,4HCON=,F10.2//)	3049	
C -----	3050	
C SECOND DEGREE TREND-SURFACE CONTOUR MAP	3052	
C -----	3053	
DX=(XR-XL)/HORZ	3054	
DY=(YB-YT)/VERT	3055	
IHORZ=HORZ	3056	
IVERT=VERT	3057	
DO 1 I=1,IVERT	3058	
RI=I	3059	
DO 2 J=1,IHORZ	3060	
RJ=J		
W(J)=A*DX*RJ*DX*RI+D		
IF(W(J),LT,REF) GO TO 3	3062	
XX=(W(J)-REF)/CON	3063	

```

IX=XX          3064
IA=MUD(IX,20) 3065
CV(JJ)=PLUS(IA+1) 3066
GO TO 2        3067
3 YY=(REF-W(J))/CON 3068
IY=YY          3069
IB=MUD(IY,20) 3070
CV(JJ)=MINUS(IB+1) 3071
2 CONTINUE     3072
WRITE(6, 95)(CV(K),K=1,IH0RZ) 3073
95 FORMAT(1HT,132A1) 3074
1 CONTINUE     3075
C -----
C COMPUTE RESIDUAL VALUES
C -----
DO 431 I= 1,K 3076
ZTRENU(I)=A*X(I)*X(I)+B*X(I)*Y(I)+C*Y(I)*Y(I)+D 3077
431 RESID(I)=Z(I)-ZTREND(I) 3078
      WRITE (6,606) 3079
606 FORMAT(1H1,51H      X      Y      Z      ZTREND 2ND RESID) 3080 2
      DO 432 I=1,K 3081
432 WRITE(6,607) X(I),Y(I),Z(I),ZTREND(I),RESID(I) 3082
607 FORMAT(1H ,5F10,1) 3083
102 RETURN     3084
      END          3085
                           3086
                           3087
                           3088

```

```

C 3RD DEGREE TREND SURFACE W/ 3RD DEGREE RESIDUALS      3001   3
C -----      3002
C -----      3003
C -----      3004
C -----      3005   3
C -----      3006   3
C -----      3007
C -----      3008
C -----      3009
C -----      3010
C -----      3011
C -----      3012
C -----      3013
C -----      3014
C -----      3015
C -----      3016
C -----      3017
C -----      3018
C -----      3019
C SET DEP VARIABLES = 0.0      3020
C -----      3021
C -----      302201 3
X1 =0.0      302202 3
X2 =0.0      302203 3
X3 =0.0      302204 3
X4 =0.0      302205 3
X5 =0.0      302206 3
X6 =0.0      302207 3
Y1 =0.0      302208 3
Y2 =0.0      302209 3
Y3 =0.0      302210 3
Y4 =0.0      302211 3
Y5 =0.0      302212 3
Y6 =0.0      302213 3
XY =0.0      302214 3
X2Y =0.0      302215 3
XY2 =0.0      302216 3
X3Y =0.0      302217 3
X2Y2=0.0      302218 3
XY3 =0.0      302219 3
X4Y =0.0      302220 3
X3Y2=0.0      302221 3
X2Y3=0.0      302222 3
XY4 =0.0      302223 3
X5Y =0.0      302224 3
X4Y2=0.0      302225 3
X3Y3=0.0      302226 3
X2Y4=0.0      302227 3
XY5 =0.0      302228 3
Z1 =0.0      302229 3
ZX =0.0      302230 3
ZY =0.0      302231 3
ZX2 =0.0      302232 3
ZXY =0.0      302233 3
ZY2 =0.0      302234 3
ZX3 =0.0

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```

ZX2Y=0.0          302235 3
ZY2=0.0          302236 3
ZY3 =0.0          302237 3
C -----
C MAKE SUMMATIONS
C -----
DO 100 I=1,K      3023
X1 = X1+X(I)      3024
X2 = X2+X(I)*X(I) 3025
X3 = X3+X(I)*X(I)*X(I) 3026
X4 = X4+X(I)*X(I)*X(I)*X(I) 302701 3
X5 = X5+X(I)*X(I)*X(I)*X(I)*X(I) 302702 3
X6 = X6+X(I)*X(I)*X(I)*X(I)*X(I)*X(I) 302703 3
Y1 = Y1+Y(I)      302704 3
Y2 = Y2+Y(I)*Y(I) 302705 3
Y3 = Y3+Y(I)*Y(I)*Y(I) 302706 3
Y4 = Y4+Y(I)*Y(I)*Y(I)*Y(I) 302707 3
Y5 = Y5+Y(I)*Y(I)*Y(I)*Y(I)*Y(I) 302708 3
Y6 = Y6+Y(I)*Y(I)*Y(I)*Y(I)*Y(I)*Y(I) 302709 3
XY = XY+X(I)*Y(I) 302710 3
X2Y = X2Y+X(I)*X(I)*Y(I) 302711 3
XY2 = XY2+X(I)*Y(I)*Y(I) 302712 3
X3Y = X3Y+X(I)*X(I)*X(I)*Y(I) 302713 3
X2Y2= X2Y2+X(I)*X(I)*Y(I)*Y(I) 302714 3
XY3 = XY3+X(I)*Y(I)*Y(I)*Y(I) 302715 3
X4Y = X4Y+X(I)*X(I)*X(I)*X(I)*Y(I) 302716 3
X3Y2= X3Y2+X(I)*X(I)*X(I)*Y(I)*Y(I) 302717 3
X2Y3= X2Y3+X(I)*X(I)*Y(I)*Y(I)*Y(I) 302718 3
XY4 = XY4+X(I)*Y(I)*Y(I)*Y(I)*Y(I) 302719 3
X5Y = X5Y+X(I)*X(I)*X(I)*X(I)*X(I)*Y(I) 302720 3
X4Y2= X4Y2+X(I)*X(I)*X(I)*X(I)*Y(I)*Y(I) 302721 3
X3Y3= X3Y3+X(I)*X(I)*X(I)*Y(I)*Y(I)*Y(I) 302722 3
X2Y4= X2Y4+X(I)*X(I)*Y(I)*Y(I)*Y(I)*Y(I) 302723 3
XY5 = XY5+X(I)*Y(I)*Y(I)*Y(I)*Y(I)*Y(I) 302724 3
Z1 = Z1+Z(I)      302725 3
ZX = ZX+Z(I)*X(I) 302726 3
ZY = ZY+Z(I)*Y(I) 302727 3
ZX2 = ZX2+Z(I)*X(I)*X(I) 302728 3
ZXY = ZXY+Z(I)*X(I)*Y(I) 302729 3
ZY2 = ZY2+Z(I)*Y(I)*Y(I) 302730 3
ZX3 = ZX3+Z(I)*X(I)*X(I)*X(I) 302731 3
ZX2Y= ZX2Y+Z(I)*X(I)*X(I)*Y(I) 302732 3
ZXY2= ZXY2+Z(I)*X(I)*Y(I)*Y(I) 302733 3
ZY3 = ZY3+Z(I)*Y(I)*Y(I)*Y(I) 302734 3
100 CONTINUE        302735 3
C -----
C FILL ARRAY
C -----
RK=K                302736 3
AA(1,1)=RK          302737 3
AA(1,2)=X1          303301 3
AA(1,3)=Y1          303302 3
AA(1,4)=X2          303303 3
AA(1,5)=XY          303304 3
AA(1,6)=Y2          303305 3

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AA(1,7)=X3	303307	3
AA(1,8)=X2Y	303308	3
AA(1,9)=XY2	303309	3
AA(1,10)=Y3	303310	3
AA(2,1)=X1	303311	3
AA(2,2)=X2	303312	3
AA(2,3)=XY	303313	3
AA(2,4)=X3	303314	3
AA(2,5)=X2Y	303315	3
AA(2,6)=XY2	303316	3
AA(2,7)=X4	303317	3
AA(2,8)=X3Y	303318	3
AA(2,9)=X2Y2	303319	3
AA(2,10)=XY3	303320	3
AA(3,1)=Y1	303321	3
AA(3,2)=XY	303322	3
AA(3,3)=Y2	303323	3
AA(3,4)=X2Y	303324	3
AA(3,5)=XY2	303325	3
AA(3,6)=Y3	303326	3
AA(3,7)=X3Y	303327	3
AA(3,8)=X2Y2	303328	3
AA(3,9)=XY3	303329	3
AA(3,10)=Y4	303330	3
AA(4,1)=X2	303331	3
AA(4,2)=X3	303332	3
AA(4,3)=X2Y	303333	3
AA(4,4)=X4	303334	3
AA(4,5)=X3Y	303335	3
AA(4,6)=X2Y2	303336	3
AA(4,7)=X5	303337	3
AA(4,8)=X4Y	303338	3
AA(4,9)=X3Y2	303339	3
AA(4,10)=X2Y3	303340	3
AA(5,1)=XY	303341	3
AA(5,2)=X2Y	303342	3
AA(5,3)=XY2	303343	3
AA(5,4)=X3Y	303344	3
AA(5,5)=X2Y2	303345	3
AA(5,6)=XY3	303346	3
AA(5,7)=X4Y	303347	3
AA(5,8)=X3Y2	303348	3
AA(5,9)=X2Y3	303349	3
AA(5,10)=XY4	303350	3
AA(6,1)= Y2	303351	3
AA(6,2)= XY2	303352	3
AA(6,3)= Y3	303353	3
AA(6,4)= X2Y2	303354	3
AA(6,5)= XY3	303355	3
AA(6,6)= Y4	303356	3
AA(6,7)= X3Y2	303357	3
AA(6,8)= X2Y3	303358	3
AA(6,9)= XY4	303359	3
AA(6,10)=Y5	303360	3
AA(7,1)= X3	303361	3

AA(7,2)= X4	303362	3
AA(7,3)= X3Y	303363	3
AA(7,4)= X5	303364	3
AA(7,5)= X4Y	303365	3
AA(7,6)= X3Y2	303366	3
AA(7,7)= X6	303367	3
AA(7,8)= X5Y	303368	3
AA(7,9)= X4Y2	303369	3
AA(7,10)=X3Y3	303370	3
AA(8,1)= X2Y	303371	3
AA(8,2)= X3Y	303372	3
AA(8,3)= X2Y2	303373	3
AA(8,4)= X4Y	303374	3
AA(8,5)= X3Y2	303375	3
AA(8,6)= X2Y3	303376	3
AA(8,7)= X5Y	303377	3
AA(8,8)= X4Y2	303378	3
AA(8,9)= X3Y3	303379	3
AA(8,10)=X2Y4	303380	3
AA(9,1)= XY2	303381	3
AA(9,2)= X2Y2	303382	3
AA(9,3)= XY3	303383	3
AA(9,4)= X3Y2	303384	3
AA(9,5)= X2Y3	303385	3
AA(9,6)= XY4	303386	3
AA(9,7)= X4Y2	303387	3
AA(9,8)= X3Y3	303388	3
AA(9,9)= X2Y4	303389	3
AA(9,10)=XY5	303390	3
AA(10,1)= Y3	303391	3
AA(10,2)= XY3	303392	3
AA(10,3)= Y4	303393	3
AA(10,4)= X2Y3	303394	3
AA(10,5)= XY4	303395	3
AA(10,6)= Y5	303396	3
AA(10,7)= X3Y3	303397	3
AA(10,8)= X2Y4	303398	3
AA(10,9)= XY5	303399	3
AA(10,10)=Y6	30331003	
BB(1)= Z1	30331013	
BB(2)= ZX	30331023	
BB(3)= ZY	30331033	
BB(4)= ZX2	30331043	
BB(5)= ZXY	30331053	
BB(6)= ZY2	30331063	
BB(7)= 03 003	30331073	
BB(8)= ZX2Y	30331083	
BB(9)= ZXY2	30331093	
BB(10)=ZY3	30331103	
C -----	3034	
C SOLVE FOR COEFFICIENTS BY MATRIX INVERSION	3035	
C -----	3036	
CALL SOLVE (10,AA,BB,1,0,0,10,CDEF,IT)	3037	3
A = CDEF(1)	303801	3
B = CDEF(2)	303802	3

```

C = COEF(3) 303803 3
D = COEF(4) 303804 3
E = COEF(5) 303805 3
F = COEF(6) 303806 3
G = COEF(7) 303807 3
H = COEF(8) 303808 3
FI= COEF(9) 303809 3
FJ= COEF(10) 303810 3
C -----
C WRITE MAP HEADING
C -----
      WRITE(6,996)
996 FORMAT(1H1,88HW=A+BX+CY+DX2+EXY+FY2+GX3+HX2Y+FIXY2+FJY3
     THIRD DEGREE TREND SURFACE)
      WRITE(6,998) A,B,C
      WRITE(6,998) D,E,F,G
      WRITE(6,997) H,FI,FJ
98 FORMAT(1H , 8HWHERE A=, F15.8,5X,2HB=,F15.8,5X,2HC=,F15.8) 304301 3
998 FORMAT(2HD=,F15.8,5X,2HE=,F15.8,5X,2HF=,F15.8,5X,2HG=,F15.8) 304307 3
997 FORMAT(2HH=,F15.8,5X,3HFI=,F15.8,5X,3HFJ=,F15.8) 304308 3
      WRITE(6,97)HORZ,VERT 3044
97 FORMAT(1H ,27HARRAY DIMENSIONS ARE--HORZ=, F6.0,11H AND VERT=,F8.3045
10)
      WRITE(6,96)XL,XR,YT,YB,REF,CON 3046
96 FORMAT(1H ,3HXL=,F10.2,10X,3HXR=,F10.2,10X,3HYT=,F10.2,10X,3HYB=,
     1F10.2,10X,4HREF=,F10.2,10X,4HCON=,F10.2//) 3048
1049
C -----
C THIRD DEGREE TREND-SURFACE CONTOUR MAP 3050
C -----
      DX=(XR-XL)/HORZ 3053
      DY=(YB-YT)/VERT 3054
      IHORZ=HORZ 3055
      IVERT=VERT 3056
      DO 1 I=1,IVERT 3057
      RI=I 3058
      DO 2 J=1,IHORZ 3059
      RJ=J 3060
      W(J)= A + B*DX*RJ + C*DY*RI + D*DX*RJ*DX*RJ+E*DX*RJ*DY*RI+F*DY*RI*306101 3
      -DY*RI+G*DX*RJ*DXX*RJ*DX*RJ+H*DX*RJ*DX*RJ*DY*RI+FI*DX*RJ*DY*RI*DY*RI 306102 3
      -+FJ*DY*RI*DY*RI*DY*RI 306103 3
      IF(W(J).LT.REF) GO TO 3 3062
      XX=(W(J)-REF)/CON 3063
      IX=XX 3064
      IA=MUD(IX,20) 3065
      CV(J)=PLUS(IA+1) 3066
      GO TU 2 3067
3 YY=(REF-W(J))/CON 3068
      IY=YY 3069
      IB=MUD(IY,20) 3070
      CV(J)=MINUS(IB+1) 3071
2 CONTINUE 3072
      WRITE(6, 95)(CV(K),K=1,IHORZ) 3073
95 FORMAT(1HT,132A1) 3074
1 CONTINUE 3075
C ----- 3076

```

```

C COMPUTE RESIDUAL VALUES          3077
C -----
DO 431 I= 1,K                      3078
ZTREND(I) = A+B*X(I)+C*Y(I)+D*X(I)**2+E*X(I)*Y(I)+F*Y(I)**2+G*X(I)**3
    ***3+H*X(I)**2*Y(I)+FI*X(I)*Y(I)**2+FJ*Y(I)**3          308001 3
431 RESID(I)=Z(I)-ZTREND(I)        308002 3
      WRITE (6,606)                  3081
      606 FORMAT(1H1,51H           X       Y       Z       ZTREND 3RD=RESID)3083 3
      DO 432 I=1,K                  3084
432 WRITE(6,607) X(I),Y(I),Z(I),ZTREND(I),RESID(I)          3085
607 FORMAT(1H ,5F10.1)              3086
102 RETURN                          3087
      END                           3088

```

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SIBFTC SOLVEX SLV40000
CSOLVE LINEAR EQUATION SOLVER WITH ITERATIVE IMPROVEMENT VERSION IV SLV40010
SUBROUTINE SOLVE(NN,A,B,IN,EPS,ITMAX,X,IT) SLV40020
C SOLVES AX=B WHERE A IS NXN MATRIX AND B IS NX1 VECTOR SLV40030
C IN= SLV40040
C 1 FOR FIRST ENTRY SLV40050
C 2 FOR SUBSEQUENT ENTRIES WITH NEW B SLV40060
C 3 TO RESTORE A AND B SLV40070
C EPS AND ITMAX ARE PARAMETERS IN THE ITERATION SLV40080
C IT= SLV40090
C * =1 IF A IS SINGULAR SLV40100
C 0 IF NOT CONVERGENT SLV40110
C NUMBER OF ITERATIONS IF CONVERGENT SLV40120
C CALLS MAP SUBROUTINES ILOG2,DOT,SDOT AND DAD SLV40130
C SLV40140
C TO MODIFY DIMENSIONS, CHANGE THE NEXT 3 (NOT 2 BUT 3) CARDS. SLV40150
DIMENSION AC( 3, 3),B( 3),X( 3),AAC( 3, 3),DX( 3),R( 3), SLV40161
* Z( 3),RMC( 3),IRPC( 3) SLV40171
MA= 3 SLV40181
C MA MUST = DECLARED DIMENSION OF SYSTEM SLV40190
EQUIVALENCE(R,DX) SLV40200
GO TO (1000,2000,3000),IN SLV40210
1000 N=NN SLV40220
NM1=N-1 SLV40230
NP1=N+1 SLV40240
C SLV40250
C EQUILIBRATION SLV40260
C SLV40270
DO 510 I=1,N SLV40280
KTOP=ILOG2(A(I,1)) SLV40290
DO 503 J=2,N SLV40300
503 KTOP=MAX0(KTOP,ILOG2(A(I,J))) SLV40310
RM(I)=2.0**(-KTOP) SLV40320
DO 509 J=1,N SLV40330
509 A(I,J)=A(I,J)*RM(I) SLV40340
510 CONTINUE SLV40350
C SLV40360
C SAVE EQUILIBRATED DATA SLV40370
C SLV40380
DO 548 I=1,N SLV40390
DO 548 J=1,N SLV40400
548 AAC(I,J)=A(I,J) SLV40410
C SLV40420
C GAUSSIAN ELIMINATION WITH PARTIAL PIVOTING SLV40430
C SLV40440
DO 99 M=1,NM1 SLV40450
TOP=ABS (A(M,M)) SLV40460
IMAX=M SLV40470
DO 12 I=M,N SLV40480
IF(TOP=ABS (A(I,M)))10,12,12 SLV40490
10 TOP=ABS (A(I,M)) SLV40500
IMAX=I SLV40510
12 CONTINUE SLV40520
IF(TOP)14,13,14 SLV40530

```

```

13 IT=-1 SLV40540
C *SINGULAR* SLV40550
RETURN SLV40560
14 IRP(M)=IMAX SLV40570
23 IF(IMAX=M)29,29,24 SLV40580
24 DO 25 J=1,N SLV40590
TEMP=A(M,J)
A(M,J)=A(IMAX,J)
AC(IMAX,J)=TEMP
25 MP1=M+1 SLV40600
29 DO 33 I=MP1,N SLV40610
EM=A(I,M)/A(M,M)
A(I,M)=EM
IF(EM)31,33,31 SLV40620
31 DO 32 J=MP1,N SLV40630
32 A(I,J)=A(I,J)-A(M,J)*EM SLV40640
33 CONTINUE SLV40650
99 CONTINUE SLV40660
IRP(N)=N SLV40670
IF (A(N,N))120,113,120 SLV40680
113 IT=-1 SLV40690
RETURN SLV40700
120 CONTINUE SLV40710
C STORAGE FOR A NOW CONTAINS TRIANGULAR L AND U SO THAT (L+I)*U=A SLV40720
C DUPLICATE INTERCHANGES IN DATA SLV40730
C DO 229 I=1,N SLV40740
IP=IRP(I)
IF(I=IP)221,229,221 SLV40750
221 DO 222 J=1,N SLV40760
TEMP=AA(I,J)
AA(I,J)=AA(IP,J)
222 AA(IP,J)=TEMP SLV40770
229 CONTINUE SLV40780
C PROCESS RIGHT HAND SIDE SLV40790
C 2000 CONTINUE SLV40800
DO 601 I=1,N SLV40810
601 B(I)=B(I)*RM(I)
DO 609 I=1,NM1 SLV40820
IP=IRP(I)
TEMP=B(I)
B(I)=B(IP)
B(IP)=TEMP SLV40830
609 CONTINUE SLV40840
C SOLVE FOR FIRST APPROXIMATION TO X SLV40850
C 199 DO 200 I=1,N SLV40860
200 Z(I)=SDOT(I=1,A(I,1),MA,Z(1),1,-B(I))
DO 201 K=1,N SLV40870
I=NP1-K
201 X(I)=SDOT(N=I,A(I,I+1),MA,X(I+1),1,-Z(I))/A(I,I) SLV40880

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```

C      ITERATIVE IMPROVEMENT          SLV41090
C
C      IF(ITMAX)370,370,300           SLV41100
300  TOP=0.0                         SLV41110
      DO 303 I=1,N                     SLV41120
      303  TOP=AMAX1(TOP,ABS(X(I)))   SLV41130
      EPSX=EPS*TOP                   SLV41140
      DO 369 IT=1,ITMAX              SLV41150
      FIND RESIDUALS                SLV41160
      DO 319 I=1,N                   SLV41170
      319  R(I)=DOT(N,AA(I,1),MA,X(1),1,-B(I))  SLV41180
C      FIND INCREMENT               SLV41190
      DO 329 I=1,N                   SLV41200
      329  Z(I)=SDOT(I=1,A(I,1),MA,Z(1),1,-R(I))  SLV41210
      DO 339 K=1,N                   SLV41220
      339  UX(I)=SDOT(N=I,A(I,I+1),MA,DX(I+1),1,-Z(I))/A(I,I)  SLV41230
C      INCREMENT AND TEST CONVERGENCE  SLV41240
      TOP=0.0                         SLV41250
      DO 342 I=1,N                   SLV41260
      TEMP=X(I)                      SLV41270
      X(I)=DAD(X(I),DX(I))          SLV41280
      DELX=ABS(X(I)-TEMP)            SLV41290
      TOP=AMAX1(TOP,DELX)
342    CONTINUE                      SLV41300
      IF(TOP=EPSX)381,381,369       SLV41310
369    CONTINUE                      SLV41320
370    IT=0                          SLV41330
381    RETURN                         SLV41340
C
C      RESTURE A AND B             SLV41350
C
3000  CONTINUE                      SLV41360
      DO 709 K=1,N                   SLV41370
      709  I=NP1-K                  SLV41380
      IP=IRP(I)                     SLV41390
      IF(I=IP)701,709,701           SLV41400
701    TEMP=B(I)                    SLV41410
      B(I)=B(IP)                   SLV41420
      B(IP)=TEMP                   SLV41430
      DO 702 J=1,N                   SLV41440
      702  TEMP=AA(I,J)              SLV41450
      AA(I,J)=AA(IP,J)             SLV41460
      AA(IP,J)=TEMP                SLV41470
702    CONTINUE                      SLV41480
      DO 729 I=1,N                   SLV41490
      729  B(I)=B(I)/RM(I)          SLV41500
      DO 729 J=1,N                   SLV41510
      729  A(I,J)=AA(I,J)/RM(I)   SLV41520
729    CONTINUE                      SLV41530
      RETURN                         SLV41540
      END                           SLV41550
$IBMAP DOT      84                 SLV41560
*     DOT AND FRIENDS          ROUTINES FOR USE WITH SOLVE
*                                         DOT40000
                                         DOT40010

```

ENTRY	DOT (N,A(1),MA,B(1),MB,C)	DOUBLE INNER PRODUCT	DOT40020	
ENTRY	SDOT (N,A(1),MA,B(1),MB,C)	INNER PRODUCT	DOT40030	
ENTRY	ILOG2 (A)	FLOATING POINT EXPONENT	DOT40040	
ENTRY	DAD (A,B)	ADD WITH ROUND	DOT40050	
*			DOT40060	
SNAD	MACHU	M STORE NEGATIVE OF ADDRESS IN DECREMENT	DOT40070	
	SUB	$\pm 0100000$ COMPLEMENT IF POSITIVE	DOT40080	
	ALS	18	DOT40090	
	STD	M	DOT40100	
	ENDM	SNAD	DOT40110	
*			DOT40120	
DOT	SAVE	1,2,4	DOT40130	
	STZ	S	DOT40140	
	STZ	S+1	DOT40150	
	CLA*	8,4	DOT40160	
	LDQ	C+1	DOT40170	
	STO	C	DOT40180	
	CLA*	3,4	DOT40190	
	TZE	NONE	SKIP LOOP IF N = 0	DOT40200
	STO	N	DOT40210	
	CLA	4,4	BASE ADDRESS OF A	DOT40220
	PAC	,1	$X_1 = \text{BASE OF } A$	DOT40230
	CLA*	5,4	MA	DOT40240
	SNAU	MA	DOT40250	
	CLA	6,4	BASE ADDRESS OF B	DOT40260
	PAC	,2	$X_2 = \text{BASE OF } B$	DOT40270
	CLA*	7,4	MB	DOT40280
	SNAD	MB	DOT40290	
	LXA	N,4	$X_4 = N$	DOT40300
LOOP	LDQ	0,1	A(I)	DOT40310
	FMP	0,2	B(I)	DOT40320
	DFAD	S	DOT40330	
	DST	S	DOT40340	
MA	TXI	*+1,1,*	$(X_1) = (X_1) + MA$	DOT40350
MB	TXI	*+1,2,*	$(X_2) = (X_2) + MB$	DOT40360
	TIK	LOOP,4,1	END OF MAIN LOOP	DOT40370
NONE	DFAD	C	DOT40380	
	FRN		DOT40390	
	RETURN	DOT	DOT40400	
*			DOT40410	
SDOT	SAVE	1,2,4	DOT40420	
	STZ	S	DOT40430	
	CLA*	8,4	DOT40440	
	STO	C	DOT40450	
	CLA*	3,4	DOT40460	
	TZE	SNONE	DOT40470	
	STO	N	DOT40480	
	CLA	4,4	DOT40490	
	PAC	,1	DOT40500	
	CLA*	5,4	DOT40510	
	SNAU	SMA	DOT40520	
	CLA	6,4	DOT40530	
	PAC	,2	DOT40540	
	CLA*	7,4	DOT40550	
	SNAU	SMB	DOT40560	

	LXA	N,4	DOT40570
SLOOP	LDQ	0,1	DOT40580
	FMP	0,2	DOT40590
	FAD	S	DOT40600
	STO	S	DOT40610
SMA	TXI	*+1,1,**	DOT40620
SMB	TXI	*+1,2,**	DOT40630
	TIK	SLOOP,4,1	DOT40640
SNONE	FAD	C	DOT40650
	RETURN	SDOT	DOT40660
*			DOT40670
ILOG2	CAL*	3,4	DOT40680
	ANA	=0377000000000	DOT40690
	SUB	=0200000000000	DOT40700
	ARS	27	DOT40710
	TRA	1,4	DOT40720
*			DOT40730
DAD	CLA*	3,4	DOT40740
	FAD*	4,4	DOT40750
	FRN		DOT40760
	TRA	1,4	DOT40770
*			DOT40780
	EVEN		DOT40790
C	PZE		DOT40800
	PZE		DOT40810
S	PZE		DOT40820
	PZE		DOT40830
N	PZE		DOT40840
	END		DOT40850

120.0 58.0 0.0 120.0 0.0 80.0 30.0 0.5  
184

0.0	2.2	32.4
10.0	2.2	32.4
20.0	2.2	33.4
30.0	2.2	33.2
40.0	2.2	33.7
50.0	2.2	34.0
60.0	2.2	33.4
70.0	2.2	34.9
80.0	2.2	33.3
90.0	2.2	32.8
100.0	2.2	33.1
110.0	2.2	32.6
120.0	2.2	32.7
0.	7.6	32.2
10.	7.6	32.4
20.	7.6	33.4
30.	7.6	34.9
40.	7.6	35.4
50.	7.6	35.9
60.	7.6	34.7
70.	7.6	33.7
80.	7.6	32.9
90.	7.6	33.0
100.	7.6	33.7
110.	7.6	33.8
120.	7.6	32.8
0.	13.2	34.0
10.	13.2	34.4
20.	13.2	34.9
30.	13.2	36.1
40.	13.2	36.3
46.	13.2	36.7
50.	13.2	35.9
60.	13.2	34.4
70.	13.2	35.0
80.	13.2	34.0
90.	13.2	33.0
100.	13.2	33.9
110.	13.2	34.3
120.	13.2	33.7
0.	20.	33.9
10.	20.	34.9
20.	20.	34.4
30.	20.	35.9
40.	20.	37.1
50.	20.	37.1
60.	20.	36.1
70.	20.	35.6
80.	20.	34.9
90.	20.	33.4
100.	20.	32.8
110.	20.	34.4
120.	20.	33.5

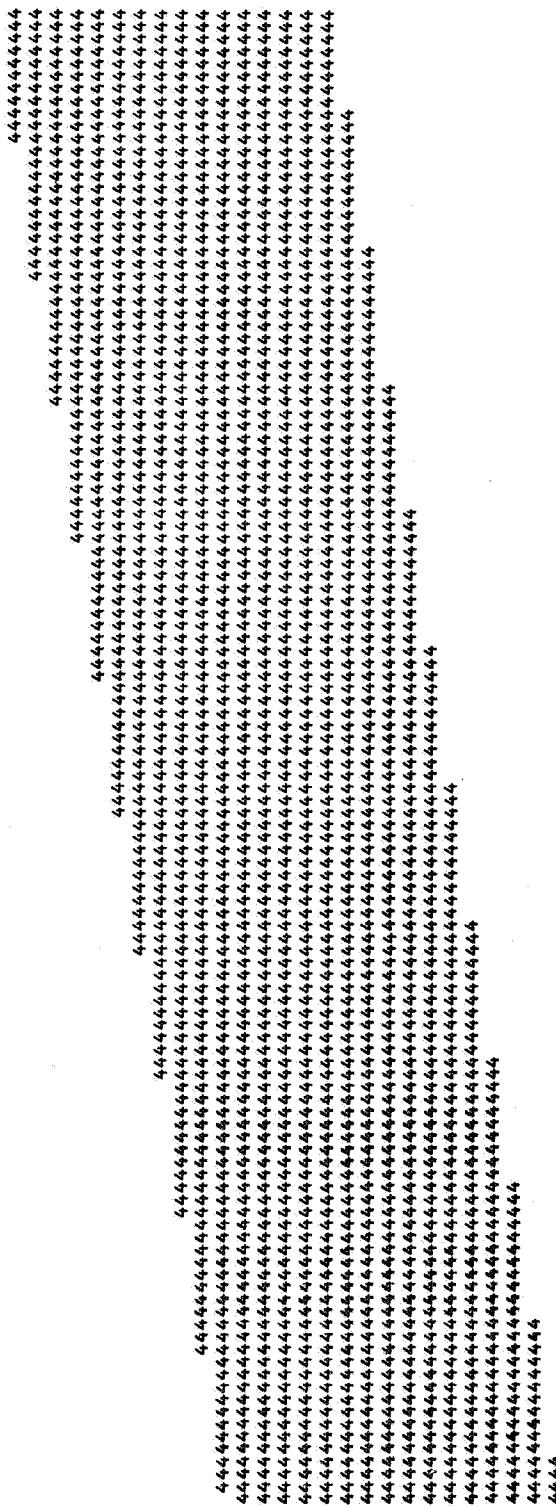
310PAA

310PAB

310PAC

310PAD

X	Y	Z	ZTREND	1ST-RESID
C.	2.2	32.4	34.8	-2.4
10.0	2.2	32.4	34.8	-2.4
20.0	2.2	33.4	34.8	-1.4
30.0	2.2	33.2	34.8	-1.6
40.0	2.2	33.7	34.7	-1.0
50.0	2.2	34.0	34.7	-0.7
60.0	2.2	33.4	34.7	-1.3
70.0	2.2	34.9	34.6	0.3
80.0	2.2	33.3	34.6	-1.3
90.0	2.2	32.8	34.6	-1.8
100.0	2.2	33.1	34.6	-1.5
110.0	2.2	32.6	34.5	-1.9
120.0	2.2	32.7	34.5	-1.8
0.	7.6	32.2	34.7	-2.5
10.0	7.6	32.4	34.7	-2.3
20.0	7.6	33.4	34.7	-1.3
30.0	7.6	34.9	34.6	0.3
40.0	7.6	35.4	34.6	0.8
50.0	7.6	35.9	34.6	1.3
60.0	7.6	34.7	34.6	0.1
70.0	7.6	33.7	34.5	-0.8
80.0	7.6	32.9	34.5	-1.6
90.0	7.6	33.0	34.5	-1.5
100.0	7.6	33.7	34.4	-0.7
110.0	7.6	33.8	34.4	-0.6
120.0	7.6	32.8	34.4	-1.6
C.	13.2	34.0	34.6	-0.6
10.0	13.2	34.4	34.6	-0.2
20.0	13.2	34.9	34.5	0.4
30.0	13.2	36.1	34.5	1.6
40.0	13.2	36.3	34.5	1.8
46.0	13.2	36.7	34.5	2.2
50.0	13.2	35.9	34.5	1.4
60.0	13.2	34.4	34.4	-0.0
70.0	13.2	35.0	34.4	0.6
80.0	13.2	34.0	34.4	-0.4
90.0	13.2	33.0	34.3	-1.3
100.0	13.2	33.9	34.3	-0.4
110.0	13.2	34.3	34.3	0.0
120.0	13.2	33.7	34.3	-0.6
C.	20.0	33.9	34.5	-0.6
10.0	20.0	34.9	34.4	0.5
20.0	20.0	34.4	34.4	0.0
30.0	20.0	35.9	34.4	1.5
40.0	20.0	37.1	34.3	2.8
50.0	20.0	37.1	34.3	2.8
60.0	20.0	36.1	34.3	1.8
70.0	20.0	35.6	34.3	1.3
80.0	20.0	34.9	34.2	0.7
90.0	20.0	33.4	34.2	-0.8
100.0	20.0	32.8	34.2	-1.4
110.0	20.0	34.4	34.1	0.3
120.0	20.0	33.5	34.1	-0.6
C.	27.2	32.7	34.3	-1.6
10.0	27.2	33.2	34.3	-1.1
20.0	27.2	34.9	34.2	0.7
30.0	27.2	35.4	34.2	1.2
40.0	27.2	37.1	34.2	2.9
44.0	27.2	37.2	34.2	3.0

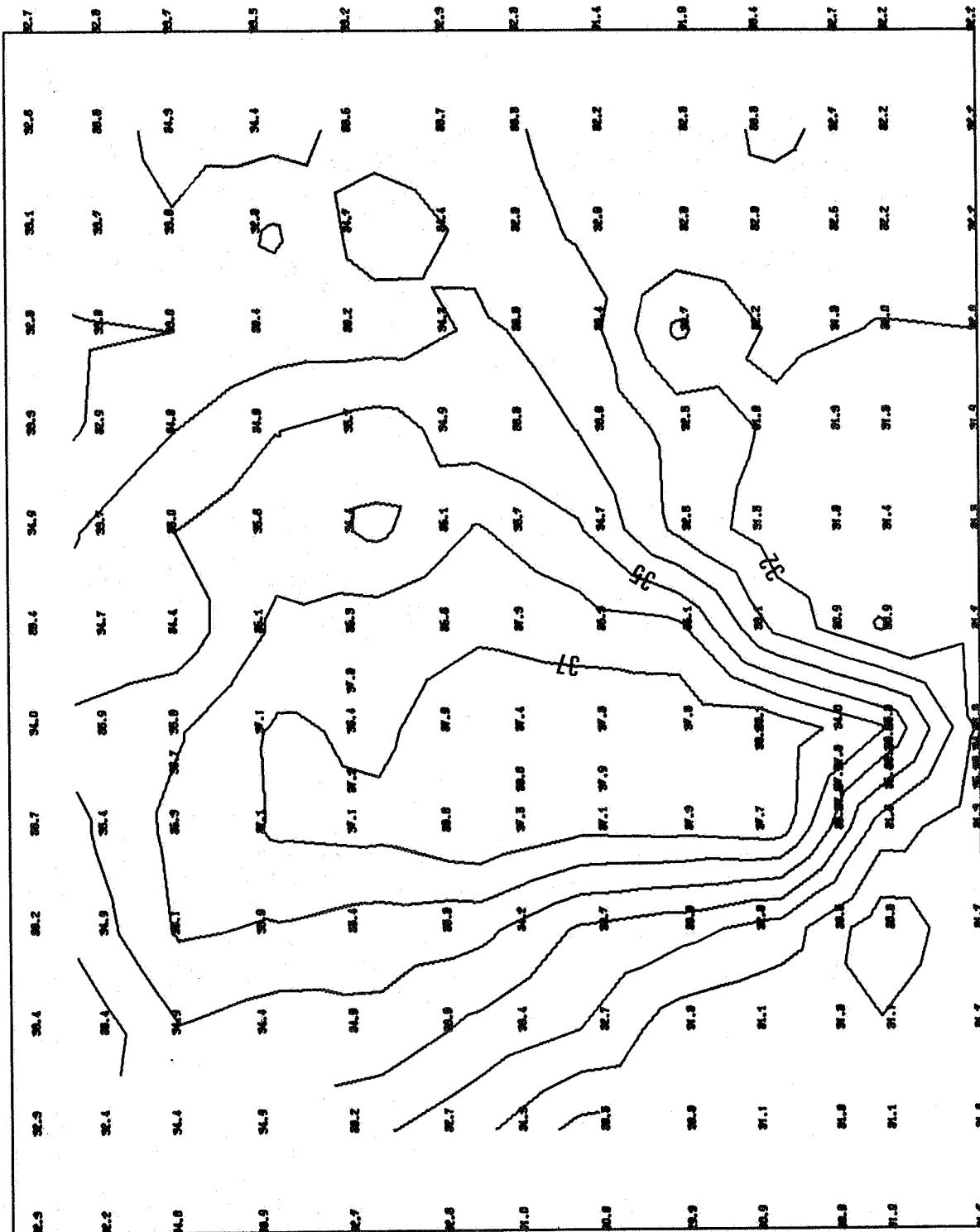




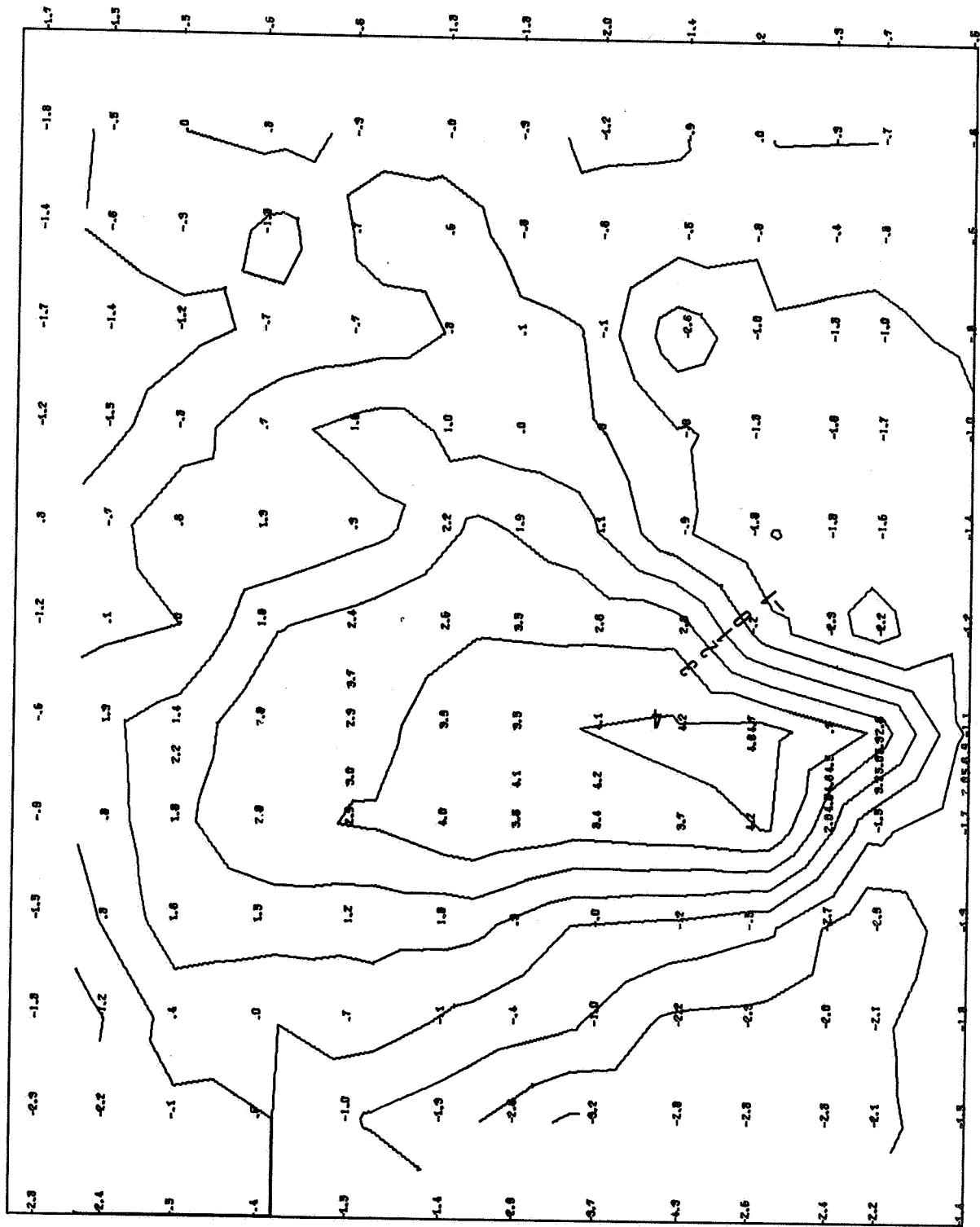
```

W=A+BX+CY+DX^2+EXY+F*Y^2+GX^3+HX^2*F*XY+JY^3
WHERE A= 3C+24B+0.212 B= 0.22954420 C= 0.18988518
D= -0.00386152 E= 0.00043566 F= -0.00546198 G= 0.00001717
H= -0.00000C340 F1= 0.00000128 F2= 0.00003555 G1= 0.00001717
ARRAY DIMENSIONS ARE--HORZ= 120. AND VERT= 58.
XL= 0. XR= 120.00 YT= 0. YB= 80.00

```

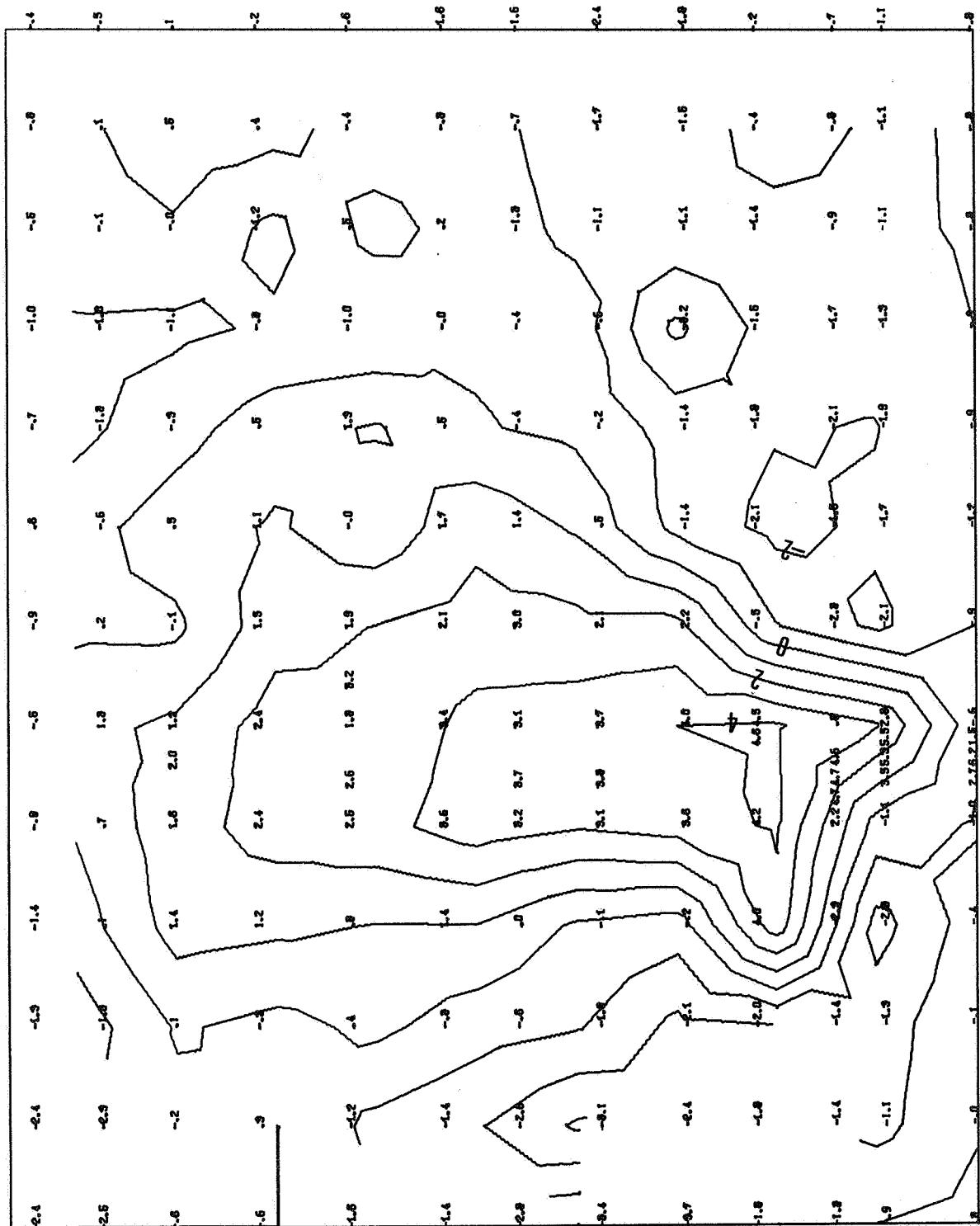


IRSATS -- APPARENT TEMPERATURES



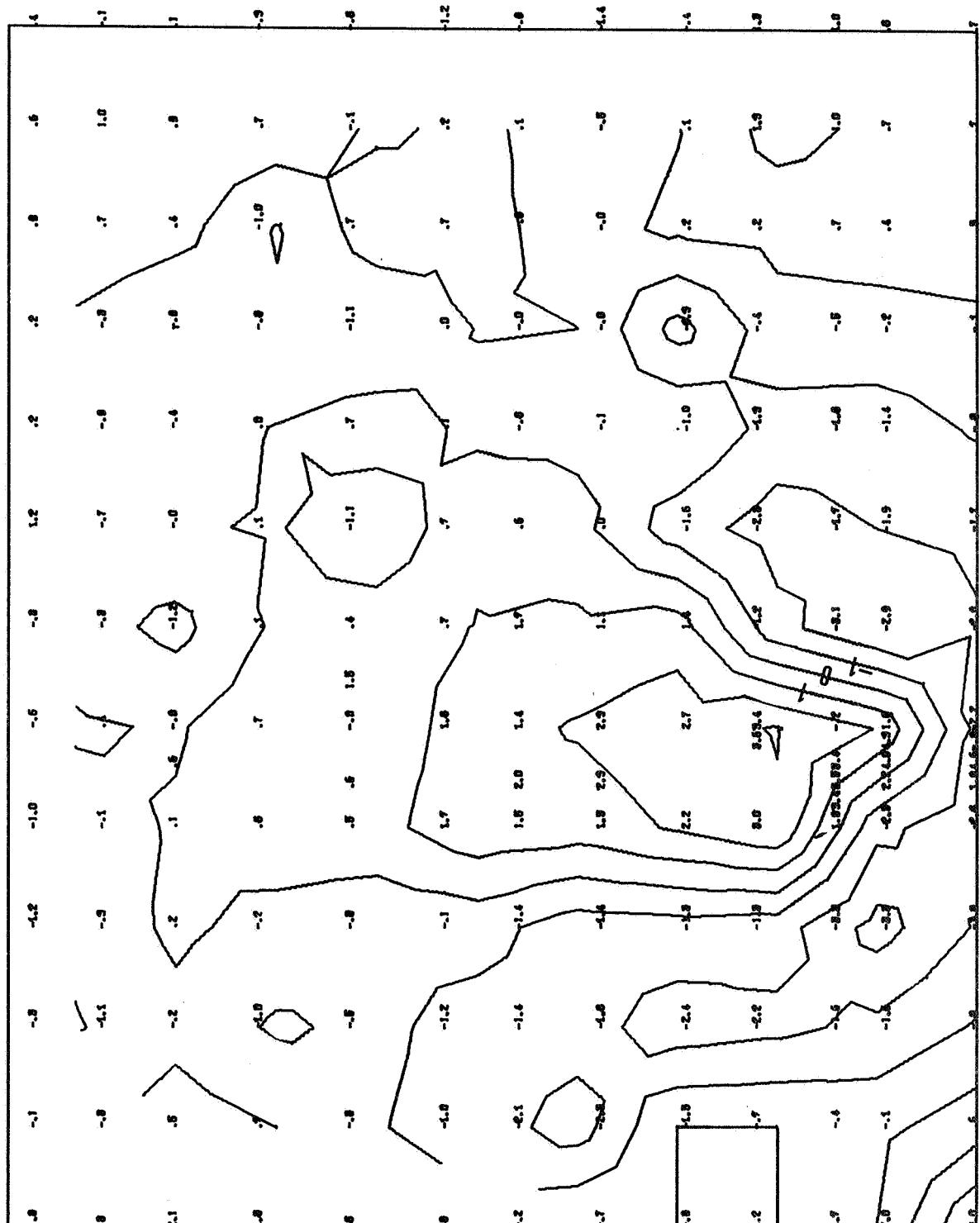
1 INCH = 10.000 MM.

IRSATS -- FIRST DEGREE RESIDUALS



1 INCH = 10.000 MM.

SRTS -- SECOND DEGREE RESIDUALS



1 INCH = 10.000 MM.

IRSTATS -- THIRD DEGREE RESIDUALS

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